

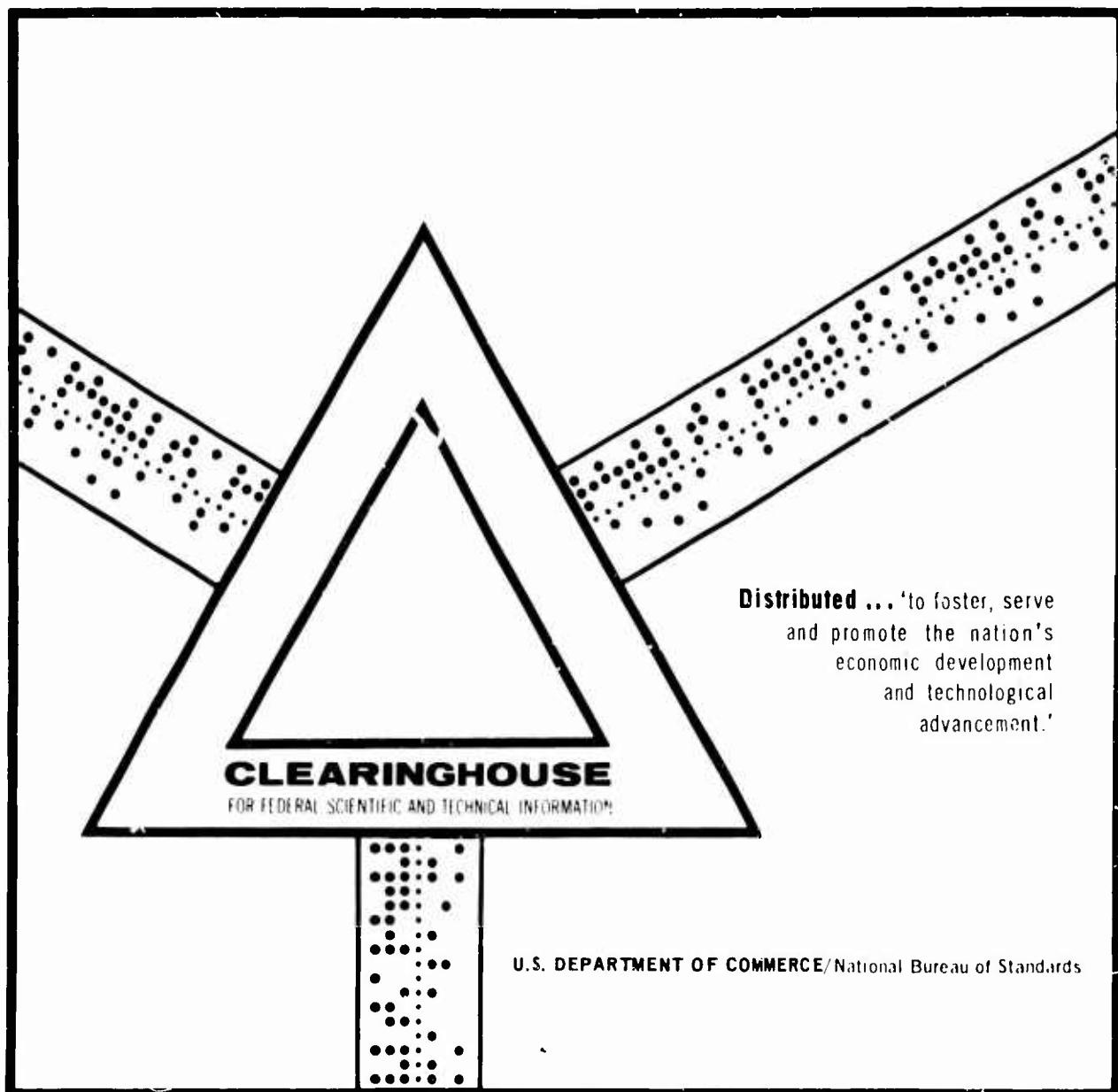
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AIRCRAFT PARACHUTE FLARE SIMULATION

Joseph J. Angotti

Naval Ammunition Depot
Crane, Indiana

1 October 1969



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NAVAL AMMUNITION DEPOT
CRANE, INDIANA

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AIRCRAFT PARACHUTE

FLARE SIMULATION

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ABSTRACT

This report presents a computer program written in Fortran IV for the IBM 360 that is a simulation of the illumination on the ground during the descent of an aircraft parachute flare from ignition to burn out. The effect of air density on the velocity is taken into account by a numerical technique. The illumination on horizontal and vertical surfaces on the ground are considered. For the surface of interest the area consisting of those points having at least a certain value of illumination is computed. The program searches for the ignition altitude for which this area is maximized over the burn time, finds the ignition altitude for which the flare burns out at a chosen altitude, or simulates the descent with ignition at a chosen altitude. Atmospheric transmission is not considered in this report.

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I. INTRODUCTION

This report presents a computer program written in Fortran IV for the IBM 350 that is a simulation of the descent of an aircraft parachute flare from ignition to burn out.

The assumptions made in the simulation are:

1. The flare is considered to be a point source of light.
2. The candlepower of the flare is constant throughout the burning time.
3. The burning rate of the flare is constant throughout the burning time.
4. The flares descend vertically in a straight line.
5. The acceleration of gravity is constant and equals 32.174 ft/sec².
6. Air density variation with altitude above sea level is given by

$$\rho(H) = .07513 \exp(-.000031582 H)$$

where $\rho(H)$ is the air density in lbs/ft³ and H is the altitude in feet.

7. The drag force on the flare due to air resistance is proportional to the square of the velocity, i.e., $F = KV^2$.
8. The drag constant is not affected by the loss of mass.
9. The ground is a flat surface.

Two types of surfaces are considered. The first is a horizontal surface on the ground. The illumination on this surface is

$$E_H = \frac{I}{D^2} \cos \theta$$

where I is the candlepower, D is the distance from the flare to a point on the ground, and θ is the angle between the line D and the normal to the ground.

The second surface is a vertical surface at ground level. The illumination on this surface is

$$E_V = \frac{I}{D^2} \sin \theta.$$

The program searches for the ignition altitude which results in a burn out at a chosen altitude or which produces the maximum area illuminated to at least a chosen value over the burn time. A run also can be obtained for any chosen ignition altitude.

A listing of the program and a sample printout is in the appendix.

II. DERIVATION OF EQUATIONS

A. Determination of Altitude During Descent

For the case of variable mass, variable air density, and drag proportional to the square of the velocity, the differential equations of motion have no exact solutions. Therefore, there are no simple, closed-form mathematical expressions which can be used to calculate altitude as a function of time for a descending flare system. A numerical technique used in this program is a special one-dimensional case of the method used and tested by Chipman⁽¹⁾ in a two-dimensional flight computer program.

The initial velocity at ignition is calculated as the equilibrium velocity (V) for the given altitude. Equilibrium velocity is the velocity where the weight (W) is equal to the drag force, i.e., $W = KV^2$. Solving for V we get $V = \sqrt{W/K}$, where $K = \frac{\rho(H)C_D A}{2g}$. The air density, $\rho(H)$ in lbs/ft³, is a function of altitude (H) above sea level in feet and is given by $\rho(H) = .07513 \exp(-.000031582 H)$. C_D is the drag coefficient, A is the drag area in square feet, and g is the acceleration of gravity (32.174 ft/sec²). The quantity $C_D A/2g$ is used in the computer program as DK (the drag constant). The next section describes a method of computing DK .

By substituting the expression for K into $V = \sqrt{W/K}$
 we get the equation for the initial velocity: $V = -\sqrt{\frac{W}{\rho(H)DK}}$,

where H is the ignition altitude above sea level. Since the positive direction is defined to be up, the descent velocity is made a negative quantity. To find the altitude and descent velocity during descent a numerical technique is used which involves making approximate computations over small intervals of time. Following is a description of the iteration scheme used in the program.

Let V equal the velocity at the beginning of an interval of time Δt . Two forces, drag in the positive direction and weight in the negative direction, are acting to produce an acceleration. The total force (F) is $-W+KV^2$. By substituting in the equation $a = F/m$ we get $a_1 = \frac{-W+KV^2}{W/g}$ or $a_1 = -g + \frac{KgV^2}{W}$ for the acceleration at the beginning of the interval.

Letting $Z = Kg/W$, we have $a_1 = -g + ZV^2$. Assuming this acceleration remains constant during the interval a first approximation to the velocity at the end of the interval, found by using the equation $V_f = V_i + at$, is $V_1 = V + a_1\Delta t$. Using this velocity the approximate acceleration at the end of the interval is $a_2 = -g + ZV_1^2$. A second approximation to the velocity at the end of the interval can be found by using

the average of the acceleration at the beginning of the interval and the approximate acceleration at the end of the interval. This gives

$$v_2 = v + \left(\frac{a_1 + a_2}{2} \right) \Delta t$$

The average of the velocity at the beginning of the interval and the second approximation for the velocity at the end of the interval is used for the average velocity over the interval. Using the equation $S = S_0 + vt$, the altitude at the end of the iteration is $H = H_0 + \left(\frac{v+v_2}{2} \right) \Delta t$ where H_0 is the altitude at the beginning of the interval.

Within each interval, the air density, $\rho(H)$, is calculated based on the altitude at the beginning of the interval and the weight is corrected by subtracting the burning rate times Δt . The values at the end of an iteration replace the initial values and the process is repeated.

In the program Δt is set at 0.1 second. Since for a parachute system the descent rate is quite low, this time interval is short enough for good approximations. After every 100 iterations a printout of time, altitude, and descent velocity is given. This gives data for every 10 seconds until the end of the burning time. Time is equal to zero at ignition.

B. Computation of Drag Constant

To compute the drag constant DK, solve the equation
for the initial velocity

$$V = \sqrt{\frac{W}{\rho(H)DK}}$$

for DK. We get

$$DK = \frac{W}{\rho(H)V^2}$$

This equation holds when the system is at its equilibrium velocity
for a given altitude and weight, which is approximately true
for a parachute system. Therefore, this equation can be used
by assuming that the system will be at its average descent velocity
and at its average altitude when half the composition is burned.

Example:

Weight of Flare and Suspension 21 pounds

Weight of Composition 17 pounds

Average Descent Rate 7.5 ft./sec.

Average Altitude (above sea level) 2,000 feet

The weight when one-half of the composition is burned is
12.5 pounds. The air density at 2000 feet equals .07053.

$$DK = \frac{W}{\rho(2000)V^2} = \frac{12.5 \text{ lbs.}}{.07053 \frac{\text{lb.}}{\text{ft.}^3} \times (7.5 \text{ ft/sec})^2} = 3.1507 \text{ ft-sec}^2$$

C. Area of Illumination for a Vertical Surface

For a fixed altitude H (in feet) and flare intensity I (in candles) the illumination E (in lumens/ft²)

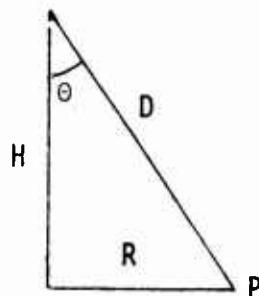


FIGURE 1

on a vertical surface at point P on the ground is given by

$$\begin{aligned} E_V &= \frac{I}{D^2} \sin \theta = \frac{I}{D^2} \cdot \frac{R}{D} \\ &= \frac{IR}{(H^2+R^2)^{3/2}} \end{aligned} \quad (1)$$

This equation can be put in the form

$$R^6 + 3H^2R^4 + \left(\frac{3E_V^2H^4 - I^2}{E_V^2} \right) R^2 + H^6 = 0 \quad (2)$$

which can be considered as a cubic equation in R^2 . Choosing a value of E_V (say E_M), the condition (see reference 2) for two positive real roots is

$$H < \sqrt{\frac{I}{\sqrt{27} E_M}} = H_C . \quad (3)$$

If the flare is above this altitude there will be no area illuminated to at least E_M and the radii are both set equal to zero. For $H < H_C$ the square root of the two positive real roots (R_1 and R_2) define an area on the ground in which the illumination on a vertical surface is greater than or equal to E_M .

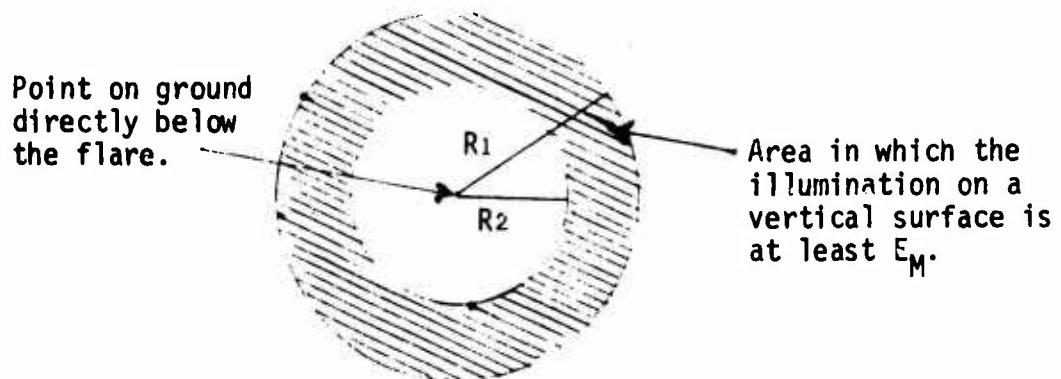


FIGURE 2

D. Area of Illumination for a Horizontal Surface

The illumination on a horizontal surface at point P is given by

$$\begin{aligned}
 E_H &= \frac{I}{D^2} \cos \theta = \frac{I}{D^2} \cdot \frac{H}{D} \\
 &= \frac{IH}{(H^2+R^2)^{3/2}} \quad (4)
 \end{aligned}$$

where H is the altitude of the flare. Choosing a value of E_H (say E_M) and solving on R we get

$$R = \sqrt{\left(\frac{IH^2/3}{E_M}\right) - H^2} \quad (5)$$

This is the radius of the area in which a horizontal surface has an illumination of at least E_M .

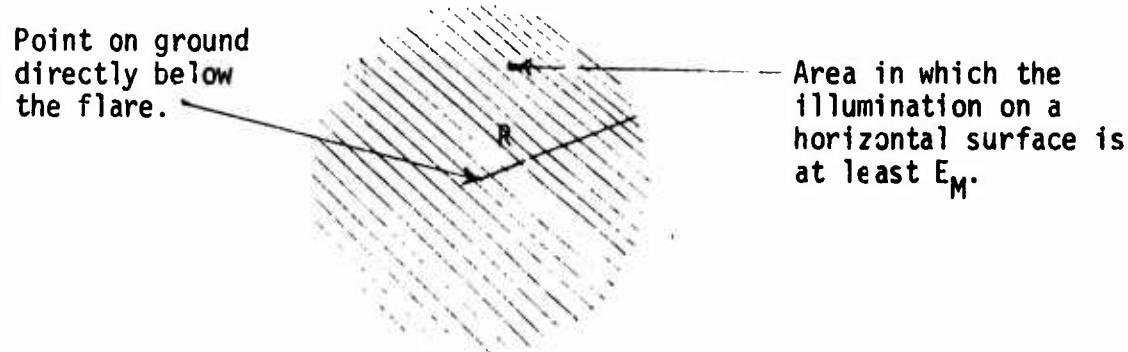
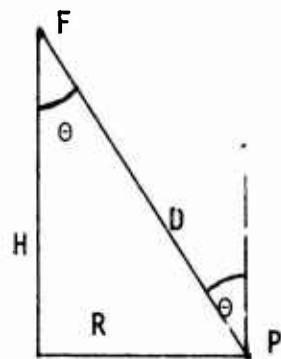


FIGURE 3

E. Optimum Ignition Altitude for a Horizontal Surface

The first step is to find the height for the particular flare intensity that will illuminate the maximum area to the required minimum illumination. This would be the ideal height to burn all of the flare. However, since the flare is descending during burning, this is impossible. Therefore, it seems reasonable that the ignition altitude should be above the optimum height

and the burn out altitude should be below the optimum height by about the same amount to yield greatest efficiency. Since descent rate varies with altitude and remaining weight, the optimum ignition altitude cannot be computed exactly.



The illumination E_H at point P from a flare with intensity I at point F is $E_H = \frac{I}{D^2} \cos \theta$. By substituting $\cos \theta = H/D$, we have $E_H = IH/D^3$. Solving for D and squaring we get $D^2 = (HI/E_H)^{2/3}$. By substituting this into the equation $R = \sqrt{D^2 - H^2}$ we get

$$R = \sqrt{\left(\frac{HI}{E_H}\right)^{2/3} - H^2}. \quad \text{To maximize } R \text{ for a given } E_H \text{ (say } E_M\text{)}$$

and I we take the derivative of R with respect to H and equate to zero (see reference 3).

$$\frac{dR}{dH} = \frac{\frac{1}{3} \left(\frac{I}{E_M}\right)^{2/3} H^{-1/3} \cdot H}{\sqrt{\left(\frac{HI}{E_M}\right)^{2/3} - H^2}} = 0$$

Solving for h we get the optimum height:

$$H_{opt} = \left[\frac{1}{3} \left(\frac{I}{E_M} \right)^{2/3} \right]^{1/4} = \frac{(I/E_M)^{1/2}}{3^{3/4}} = \frac{(I/E_M)^{1/2}}{2.279507} \quad (7)$$

In the program the approximate ignition altitude is computed by adding to the optimum height the product of the estimated average descent rate and one-half the burning time. The range for the trial ignition altitudes is found by multiplying the approximate ignition altitude by 1.25 for the upper limit and multiplying by .75 for the lower limit. The difference of these two altitudes is divided by 20 to obtain the increment between trial ignition altitudes.

Calculations are made for ignition altitudes at the upper limit first. It is possible for the altitude to be high enough that there is no area illuminated to the minimum requirement. The integration of area versus time is done by a numerical technique (the trapezoidal rule). The height is found at regular time intervals during the descent by the method described in section A of part II. After every 100 iterations, the area which is illuminated to the minimum illumination is calculated. The value of area-time for each interval is computed by multiplying the time interval by the average of the area at the beginning of the interval and the

area at the end of the interval. The total integral of area versus time is found by summing over all the burning time. The number of iterations and the time of the iterations determine the time interval for integration.

The next trial ignition altitude is found by subtracting the distance that was calculated for the increment between trial ignition altitudes. The same procedure is repeated for this trial ignition altitude. When the integral of area over the burn time for the present drop becomes less than the integral for the previous drop the ignition altitude for the previous drop is the estimate - the optimum ignition altitude for the given illumination level. The true optimum ignition altitude is then within the last increment of the estimate. A smaller interval can be found once the maximum value of the integral is past and a new set of twenty points computed.

In case the flare hits the ground while burning for any of the ignition altitudes, no lower ignition altitude is tried because the integral of area-time would only decrease.

III. INPUT TO PROGRAM

A. Data Format on Cards

<u>Card</u>	<u>FORTRAN Name</u>	<u>Columns</u>	<u>Format</u>
1	NPROG	1-2	I2
2	CD	1-10	E10.5
	TW	11-20	F10.0
	WC	21-30	F10.0
	DK	31-40	F10.0
	KOMPUT	41-45	I5
	VBAR	46-50	F5.0
	BT	51-55	F5.0
	TD	56-60	F5.0
	ITER	61-65	I5
	HV	66-70	F5.0
	ID1	71-74	A4
	ID2	75-78	A4
	ID3	79-80	A2
3	H1	1-10	F10.0
4	EMIN	1-10	F10.0
	HASL	11-20	F10.0
	KODE	21	I1

B. Explanation of Terms

The first data card contains the value of NPROG which is a code number used to designate the subroutine to be run.

<u>NPROG</u>	<u>Subroutine</u>
1	VSB1 (see section IV.B)
2	VSF1 (see section IV.B)
3	HSB1 (see section IV.B)
4	HSF1 (see section IV.B)
5	HSO (see section IV.B)

The second data card contains the flare parameters. The first parameter is the candlepower of the flare (CD). It is assumed to be a constant value from ignition to burnout. The next parameter is the total weight (TW) of the descending system. This includes the original amount of composition and the parachute system. The third parameter is the original amount of composition. Both weights are in pounds. The next parameter is the drag constant (DK). Section II.B shows how it is computed. The next variable (KOMPUT) provides two ways of reading in DK. If KOMPUT = 1 the value read in as DK is used for DK. If KOMPUT = 2 the value of DK is computed from the values of VBAR, the average velocity of the system (in feet/second), and HV, the altitude above sea level at which the system has an equilibrium velocity of VBAR ft/sec. The value of VBAR should be on the card when executing the subroutines VSB1, HSB1, and HSO since it is used to compute an estimate of the ignition altitude. The next parameter is the burn time (BT) of the flare measured in seconds. The variable TD is the time increment (in seconds) used in the calculation of the height of the flare. The variable ITER is the number of iterations used to calculate the height of the flare. The product of these two variables gives the time between printouts. The three variables ID1, ID2, ID3 are used to label the printout with 1 to 10 characters.

The third data card contains the variable H1. For the subroutines VSB1 and HSB1 this value is the burn out altitude. For the other subroutines, VSF1 and HSF1, it is the ignition altitude. This card is not required for the subroutine HSO. The altitude is measured in feet above the ground (not sea level).

The height of the ground above sea level (in feet) is the second variable on the fourth card. The first variable (EMIN) is the minimum illumination level required on the ground measured in lumens/sq.ft. The third variable (KODE) takes on integer values 0-9 and is used to obtain a run (with the same data) of one of the other subroutines, depending on which subroutine was just executed. When KODE takes on a positive value the following is indicated.

<u>NPROG</u>	<u>Subroutine to be Run</u>
1	HSB1
2	HSF1
3	VSB1
4	VSF1
5	VSF1 (at the optimum ignition altitude)

Thus, if the subroutine VSB1 is to be executed first and one wishes to obtain a run for the same data on HSB1, the value of KODE should be a positive integer between 1 and 9 and NPROG set to 1. No other subroutine will be executed if KODE = 0.

IV. DESCRIPTION OF COMPUTER PROGRAM

A. Main Program

The purpose of the main program is to read in the data and to call the indicated subroutines. The first card contains NPROG which is an integer used to indicate which subroutine is to be executed:

<u>NPROG</u>	<u>Subroutine to be Executed</u>
1	VSB1
2	VSF1
3	HSB1
4	HSF1
5	HSO

If a blank card is read the program stops.

The flare parameter card is read in next. If zero is read in as the value of ITER, the program will read in another value of NPROG. If ITER has a positive value the program then computes the drag constant and the burn rate of the flare.

The ignition altitude (if NPROG = 2 or 4) or the burn out altitude (if NPROG = 1 or 3) is then read in. This card is not needed for HSO (NPROG = 5). If zero is read in, the program will read in another flare parameter card. If a positive value is read in, the program will read in the illumination card containing the minimum illumination level, the height of the ground above sea level, and the value of

KODE. If zero is read in as the value of the illumination level the program will read in an ignition (or burn out) altitude card. If a positive value is read in, the program will call the indicated subroutine. After returning from the called subroutine the main program then executes the option indicated by the value of KODE. If KODE = 0 another illumination card is read. If KODE is a one digit, positive integer the following subroutine will be called depending on the value of NPROG.

<u>NPROG</u>	<u>Subroutine to be Run</u>
1	HSB1
2	HSF1
3	VSB1
4	VSF1
5	VSF1 (at the optimum ignition altitude)

Another illumination card is then read.

The program is set up so that a blank card can be used to control which data card is to be read in next. To stop the program after executing a set of data, four blank cards are needed. When setting up the data cards, it must be remembered what type of data card the program is looking for next. Section V shows the data set up for a sample run.

B. The Five Main Subroutines

The value of NPROG is used to indicate which of the five main subroutines is to be run by using the following code:

<u>NPROG</u>	<u>Subroutine</u>
1	VSB1
2	VSF1
3	HSB1
4	HSF1
5	HS0

The subroutines VSB1 and HSB1 search for the ignition altitude where the flare burns out at a specified altitude above the ground. VSB1 is for a vertical surface and HSB1 is for a horizontal surface. One can be executed for a set of data just run on the other by use of the variable KODE (See section III). Both can determine the ignition altitude by the third trial by making a correction to the trial ignition altitude if the burnout altitude is missed by more than half a foot. Time is set to zero at ignition. If the flare hits the ground a correction is made to the ignition altitude and the procedure started over again.

The subroutines VSF1 and HSF1 give a printout for a specified ignition altitude and illumination level for a vertical and horizontal surface respectively. The variable KODE is used to obtain a run on one subroutine with the same set of data that was run on the other (see section III). The subroutines are ended if the flare hits the ground.

The subroutine HSO searches for the ignition altitude for which the integral of the illuminated area on a horizontal surface versus time from ignition to burn out is maximized. Section II.E describes the procedure used to obtain the estimate of the optimum ignition altitude. An increment within which the true optimum ignition altitude lies is also given. The variable KODE is used to obtain a run at the estimate of the optimum ignition altitude with the same data for a vertical surface.

The subroutine ROOTS determines the radii of the illuminated area for a vertical surface (see section II.C.). The subroutine HEADER is used to printout data. RHO computes the density of the air at a specified altitude above sea level. The subroutine RALPH is part of the iteration technique used to compute the altitude of the flare (see section II.A. and Chipman⁽¹⁾).

V. SAMPLE RUNS FOR THE MK 45 AIRCRAFT PARACHUTE FLARE

A. Data Setup

Data for a sample run is shown in Table 1 on an 80-column card coding form. The data is set up according to the formats listed in section III.A. and is as follows:

Card 1:	NPROG	1	Subroutine VSBl is to be run
Card 2:	CD =	1.65E+06	Candlepower of flare = 1.65×10^6
	TW =	22.5	Total weight of system (lbs)
	WC =	17.5	Weight of composition (lbs)
	DK =	3.14382	Drag Constant
	KOMPUT =	1	DK is to be the value of the drag constant. If KOMPUT = 2, the method of section II.B. would be used to compute DK.
	VBAR =	8.	Average descent velocity (ft/sec)
	BT =	180.	Burn time (sec)
	TD =	.1	Time increment (sec)
	ITER =	100	Number of iterations for the computation of the altitude of the flare
	HV	-	Altitude at which the system has VBAR as descent velocity. Not needed since KOMPUT = 1.
	ID1, ID2, ID3 MK 45-8		Run identification for printout
Card 3:	H1 =	300.	Burn out altitude (feet) since NPROG = 1
Card 4:	EMIN =	.02	Minimum illumination level (lumens/sq.ft.)

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	HASL = 0.	Ground is at sea level
	KODE = 1	Run on HSB1 with same data desired
Card 5:	EMIN = .05	Another illumination level to be run on VSB1 for a burn out altitude of 300. The rest of the card is the same as card 4. Hence a run on HSB1 is desired.
Card 6:	EMIN = .10	Another illumination level. The rest of the card is the same as cards 4 and 5.
Card 7:	Blank	This blank card indicates that there is no more illumination levels. The program will be waiting for a burn out altitude card.
Card 8:	Blank	No more burn out altitudes, program will be looking for a candle parameter card.
Card 9:	Blank	No more candle parameters, program will be looking for another value of NPROG.
Card 10:	NPROG = 5	The optimum ignition altitude subroutine (HS0) is to be run
Card 11:	Same as Card 2	
Card 12:	EMIN = .02 HASL = 0. KODE = 1	Minimum illumination level Ground at sea level A run on VSF1 with the same data is wanted. The ignition altitude will be the optimum ignition altitude.
Card 13:	Blank	No more illumination levels. Program will be expecting an ignition (or burn out) altitude. Next card should be blank.

Card 14	Blank	No more values of H1. The program will be looking for a candle parameter card.
Card 15	Blank	No more candle parameters. Program will be looking for another value of NPROG.
Card 16	Blank	No more subroutines to be run. Terminates program.

B. Description of Printout

A listing of the Fortran IV computer program written for the IBM 360 is given in Appendix A. A sample printout for the data setup in section V.A. is given in Appendix B.

On the printout CD is the flare intensity in candles. EMIN is the minimum illumination level in lumens/sq.ft. The total weight of the system (TW) is measured in pounds and includes the weight of the parachute. The weight of the composition (WC) is measured in pounds. It is used along with the burn time (BT) in seconds to determine the burn rate. The variable DK is used to determine the velocity of the flare and depends on the cross-sectional area of the parachute and its drag constant (see section II.A.). HASL is the height of the ground above sea level.

The time after ignition is given every ten seconds. The height of the flare and its velocity is given for each point in time. The radius (for horizontal surfaces) or the radii (for vertical surfaces) is given as well as the area which has the required minimum illumination. The integral of the area

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illuminated versus time from ignition to each point in time is printed out. The average area illuminated since ignition is also computed and printed out for each point in time.

For burn out altitude of 300 feet, runs were obtained for minimum illumination levels of 0.02, 0.05, and 0.10 lumens/sq.ft. on both the vertical and horizontal surface subroutines (see section II). The optimum ignition altitude for a minimum illumination level of 0.02 lumens/sq.ft. was obtained as well as a printout for the vertical surface subroutine at the optimum ignition altitude.

9ND-NASC 5230/2 (6-65)

DATA PROCESSING CARD FORMAT

TABLE I
DATA SET-UP FOR SAMPLE RUN

13 indicates a blank care

RUDK NO. 151

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1. Chipman, Ralph, "Two-Dimensional Flight Computer Program", RDTR No. 83, NAD Crane, Indiana, 21 September 1966.
2. Korn, Granino A. and Korn, Theresa M., "Mathematical Handbook for Scientists and Engineers", McGraw-Hill, New York, 1961.
3. Laswell, John E. "Study of the Optimum Suspension of a High Intensity Parachute Flare", RDTN No. 30, NAD Crane, Indiana, 1 May 1963.

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APPENDIX A

COMPUTER PROGRAM LISTING

RDT_R No. 157

// JOB TE7P40 ILLUMINATING FLARE SIMULATION--JOSEPH J. ANGOTTI
// OPTION LINK
PHASE TE7P40,S
// EXEC FORTRAN

```

C   ILLUMINATING FLARE SIMULATION PROGRAM
COMMON T,TD,CD,EMIN,TW,WC,W,DK,HV,BT,BR,VBAR,DH,ALT,H1,H2,HC,HOPT
COMMON AREA1,AREA2,SOBT,VI,V2,G,PI,V,HASL,ROOT(3),ABAR,R
COMMON K,HI1,ITER,KOMPUT,IDL,ID2,ID3,NPROG,KODE
DOUBLE PRECISION T,TD
FORMAT(10.5,3F10.0,15,3F5.0,15,F5.0,2A4,A2)
334 FORMAT(2F10.0,11)
      G=32.174
      PI=3.141593
      6 READ(1,7)NPROG
      7 FORMAT(12)
      IF(NPROG)>8,8,9
      8 CALL EXIT
      9 READ(1,1)CD,TW,WC,DK,KOMPUT,VBAR,BT,TC,ITER,HV,IDL,IDL,IDL,IDL
      IF(ITER)>6,10
      10 GO TO (20,22),KOMPUT
      GO TO 6
      22 DK=(TW-WC/2.)/RHO(HV)/VBAR/VBAR
      20 BR=WC/BT
      GO TO (11,11,11,11,12),NPROG
      11 READ(1,33)H1
      IF(H1)<9,9,23
      23 GO TO (24,12,24,12,12),NPROG
      24 H2=H1
      H1=H1+VBAR*BT
      12 READ(1,33)EMIN,HASL,KODE
      IF(EMIN)>11,11,13
      13 HC=SQRT((2.*CD/5.*196152/EMIN)
      HOPT=SQRT((CD/EMIN)/2.27951)
      GO TO (14,15,16,17,5),NPROG
      GO TO 8
      14 CALL VSBI
      GO TO 18
      15 CALL VSFI
      GO TO 18
      16 CALL HSBI
      GO TO 18
      17 CALL HSFI
      GO TO 18
      5 CALL HSO
      18 IF(KODE)>12,12,19
      19 KODE=0
      GO TO (15,17,14,15,15),NPROG
      GO TO 8
      FNC

```

36/06/69

FORTRAN

00002

COMMON

SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
I	0000	ID	C098	EWIN	00C0	IV	0018
WC	001C	K	C020	HV	0024	B1	002C
BR	0C30	VBAR	C034	ALT	0038	H1	0040
H2	0044	HC	0048	AREA1	004C	AREA2	0054
SOAT	0058	VI	005C	G	0060	P1	0068
V	006C	HASL	0070	U74	0074	R	0084
K	0088	IH1	008C	ABAR	0090	D1	0098
ID2	009C	ID3	C0A0	KMPUT	0094		
				KODE	00A4		

CALLED SUBROUTINES

LJTAAFR	LJTACOM	LJTFXIT	EXIT	RMC	LJTSCT	SGRT	V541	V5F1	HSFI	HSB1

LABEL	LOCATION								
00001	0078	C034	C094	00006	008E	00007	00E0	00008	00F6
00009	0100	00010	018C	00022	01BC	00023	01EE	00011	022A
00023	0258	00024	0288	00012	02A4	00013	02E0	00014	0356
00015	0366	00016	0376	00017	0386	00005	0398	00018	03A0
00019	0380								

COMPILEATION COMPLETE

AMOUNT OF COMMON 300112

AMOUNT OF CORE 300112

ADDRESS BASE TABLE

0388

RDTR No. 157

RD1R No. 157

// EXEC FORTRAN

Tape OPERATING SYSTEM-V360 FORTRAN : 36JM-FD-409 27

```
SUBROUTINE VSBI
COMMON T,TD,CD,EMIN,1,TC,DR,MV,D,VBAR,D,ALT,ML,M2,HC,HOPT
COMMON AREA1,AREA2,SUBT,VI,V2,G,PI,MASL,R,DT(3),A,AR,R
COMMON K,IM1,ITER,KOMPUT,ICL,IR,03,NPROC,KODE
DOUBLE PRECISION T,TO
43 ALT=ML
      SUBT=C.
      ABAR=0.
      AREA1=0.
      T=0.
      M=TW
      CALL HEADER(1)
      V=SQRT(1/RHO(ALT+MASL)/DK)
      IF(MC-AL .GT. 21,21,22
21 ROOT(1)=J.
      ROOT(2)=0.
      CALL HEADER(6)
      GO TO 7
22 CALL ROOTS
      IF(K)331,331,63
      63 CALL HEADER(6)
      AREA1=AREA2
      7 DO 8 IT=1,ITER
      CALL RALPH
      IF(ALT)88,88,85
      85 IF(T-BT+.00001)8,89,89
      8 V=Y2
      IF(ALT)88,89,89
      89 ALT=0.
      ROOT(1)=SQRT(CD/EMIN)
      ROOT(2)=0.
      CALL HEADER(6)
      M1=M1*BT/T+M2*.5
      IM1=ML
      M1=IM1
      GO TO 43
      99 IF(MC-ALT)21,21,62
      62 CALL ROOTS
      IF(K)331,331,64
      64 CALL HEADER(6)
      AREA1=AREA2
      IF(1-BT+.00001)17,9,9
      9 DM=ALT-T-M2
      IF(ABS(DM)--.5)331,331,42
331 RETURN
      42 M1=M1-CH*.5
      IM1=ML
      M1=IM1
      GO TO 43
      ENC
```

06/06/69

185

RDTR No. 157

RDTR No. 157

// EXEC FORTRAN

TAPE OPERATING SYSTEM/360 FORTRAN 360M-F0-409 20

```
SUBROUTINE VSF1
COMMON T, TD, CD, EMIN, TW, MC, W, DK, HV, BT, BR, VBAR, DH, ALT, H1, H2, HC, HOPT
COMMON AREA1, AREA2, SOBT, VI, V2, G, PI, V, HASL, ROOT(3), ABAR, R
COMMON K, IH1, ITER, KOMPUT, ID1, ID2, ID3, NPROG, KODE
DOUBLE PRECISION T, YD
ALT=H1
SOBT=0.
ABAR=0.
AREA1=0.
T=0.
W=TW
CALL HEADER(2)
Y=-SQRT(W/RHO*(ALT+HASL)/DK)
IFI(HC-ALT)21,21,22
21 ROOT(1)=0.
ROOT(2)=0.
CALL HEADER(6)
GO TO 7
22 CALL ROOTS
IFI(K)331,331,63
63 CALL HEADER(6)
AREA1=AREA2
7 DO 8 IT=1,ITER
CALL RALPH
IFI(ALT)88,88,85
85 IF(T-BT+.0001)8,89,89
8 Y=V2
IFI(ALT)88,88,89
88 ALT=0.
ROOT(1)=SQRT(CD/EMIN)
ROOT(2)=0.
CALL HEADER(6)
GO TO 331
89 IF(HC-ALT)21,21,62
62 CALL ROOTS
IFI(K)331,331,64
64 CALL HEADER(6)
AREA1=AREA2
IFI(T-BT+.0001)7,331,331
331 RETURN
END
```

06/06/69

VSF1

0002

COMMON					
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
T	0000	ID	0000	CD	0010
MC	001C	W	0020	DK	0024
BR	0030	VBAR	0034	DH	0038
M2	0044	HC	0048	HOPT	004C
SOBT	0058	V1	005C	V2	0060
V	006C	HASL	0070	ROOT	0074
K	0088	IH1	008C	ITER	0090
ID2	009C	ID3	00A0	NPROG	00A4
SCALARS					
IT	0096	HEADER	1JTACOM	RHO	ROOTS
			1JTSSQT	SQRT	RALPH
CALLED SUBROUTINES					
LABEL	LOCATION	LABEL	LOCATION	LABEL	LOCATION
00021	00EE	00022	0112	00063	012C
30008	0180	00088	01AC	00089	01EA
00331	0246				
COMPILEATION COMPLETE			AMOUNT OF COMMON 000172	AMOUNT OF CORE 000768	ADDRESS BASE TABLE 0228

RDTR No. 15;

RDTR No. 157

// EXEC FORTRAN

TAPE OPERATING SYSTEM/360 FORTRAN 367M-FD-409 20

```
SUBROUTINE HSB1
COMMON T,TD,CD,EMIN,TW,MC,M,OK,MV,BT,BR,VBAR,DH,AL1,H1,H2,HC,HOPT
COMMON AREAL,AREA2,SDBT,V1,V2,G,PI,V,HASL,ROOT(3),ABAR,R
COMMON K,IHI,ITER,KCOMPUT,IDL,ID2,ID3,NPROC,KODE
DOUBLE PRECISION T,TD
EXPNT=2./3.

43 ALT=H1
SDBT=0.
ABAR=0.
AREAL=0.
T=0.

H=TW
CALL HEADER(3)
ARG=(CD*ALT/EMIN)**EXPNT-ALT*ALT
IF(ARG)16,16,17
16 R=0.
GO TO 18
17 R=SQRT(ARG)
18 V=-SQRT(W/RHO(ALT+HASL)/WK)
CALL HEADER(7)
AREAL=AREA2
7 DO 8 IT=1,ITER
CALL RALPH
IF(ALT)88,88,85
85 IF((T-BT+.0001)*6,89,89
8 V=V2
IF(ALT)88,88,89
88 ALT=0.
R=0.
CALL HEADER(7)
H1=H1*BT/T+H2*.5
87 IM1=H1
H1=IM1
GO TO 43
89 ARG=(CD*ALT/EMIN)**EXPNT-ALT*ALT
IF(ARG)13,13,14
13 R=0.
GO TO 15
14 R=SQRT(ARG)
15 CALL HEADER(7)
AREAL=AREA2
IF((T-BT+.0001)*7,9,9
9 DH=ALT-H2
IF(LABS(DH)-.5)331,331,42
42 H1=H1-DH*.5
GO TO 87
331 RETURN
END
```

69/94C/94

HSB1

2000

COMMON

SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
T	0000	TC	C008	CD	0010	EMIN	0014
MC	00-C	W	0020	DK	0024	HV	0026
BR	0030	VBAR	0034	DH	0038	ALT	003C
H2	0044	HC	0048	MOPT	004C	AREA1	0050
S061	0058	V1	005C	V2	0060	G	0064
V	006C	HASSL	0070	ROOT	0071	ABAR	0080
K	0088	IM1	008C	ITER	0090	KOMPUT	0094
102	009C	ID3	00A0	NPROG	00A4	KODE	101

SCALARS

SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
EXPNT	00BC	ARG	00C0	IT	00C4		

CALLED SUBROUTINES

IJTACOM	IJTARXR	HEADER	IJTSSOR	SCRT	RHO	RALPH

LABEL	LOCATION	LABEL	LOCATION	LABEL	LOCATION	LABEL	LOCATION
00043	0078	00016	00FC	00017	00FE	00018	011C
00085	017C	00008	0198	00086	01C4	00087	0202
00013	0284	00014	0296	00015	02A8	00009	02D5
00331	0312						

COMPILED COMPLETE AMOUNT OF COMMON 00G172 AMOUNT OF CORE 00156 ADDRESS BASE TABLE 02F8

RDTR No. 157

RDTR No. 157

// EXEC FORTRAN

```

SUBROUTINE HSFL
COMMON T,TD,CD,EMIN,TW,WC,DK,HV,BT,BR,VBAR,DH,ALT,HI,H2,HC,HOPT
COMMON AREAL,AREA2,SOBT,VI,V2,G,PI,V,HASL,ROOT(3),ABAR,R
COMMON K,IHL,ITER,KOMPUT,ID1,ID2,ID3,NPROG,KODE
DOUBLE PRECISION T,TD
EXPNT=2./3.

ALT=HI
SOBT=0.
ABAR=0.
AREAL=0.
T=0.
TW=TW

CALL HEADER(4)
ARG=(CD*ALT/EMIN)**EXPNT-ALT*ALT
IF(IARG)16,16,17
16 R=0.
GO TO 18
17 R=SQR(TARG)
18 V=-SQR(W/RHO(ALT+HASL)/DK)
CALL HEADER(7)
AREAL=AREA2
7 DO 8 IT=1,ITER
CALL RALPH
IF(ALT)86,88,85
85 IF(1-T-BT+.0001)8,89,89
8 V=V2
IF(ALT)88,88,89
89 ALT=0.
R=0.
CALL HEADER(7)
331 RETURN
89 ARG=(CD*ALT/EMIN)**EXPNT-ALT*ALT
11 IF(IARG)13,13,14
13 R=0.
GO TO 15
14 R=SQR(TARG)
15 CALL HEADER(7)
AREAL=AREA2
16 IF(1-T-BT+.0001)7,331,331
END

```

06/06/69

HSF1

0002

COMMON

SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
T	0000	TD	C008	CD	0010	EMIN	0014
WC	001C	W	0020	DK	0024	HV	0018
BR	0030	VBAR	0034	DH	0038	ALT	002C
H2	0044	HC	0048	HOPT	004C	AREA1	0040
SOBT	0058	V1	005C	V2	0060	G	0054
V	006C	HASL	0070	ROOT	0074	ABAR	0068
K	0088	IH1	008C	ITER	0090	KOMPI	0084
ID2	009C	ID3	00A0	NPROG	00A4	KODE	0098

SCALARS

SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
EXPNT	00AC	ARG	00B0	IT	00B4	RHO	RALPH

CALLED SUBROUTINES

IJTACOM	IJTARXR	HEADER	IJTSSQT	SORT	LOCATION	LABEL	LOCATION	LABEL	LOCATION
					0110 01E2	00018 00331	00007 00089	015A 01F4	00065 00013

AMOUNT OF COMMON 000172 AMOUNT OF CORE 000848 ADDRESS BASE TABLE 0258

RDTR No. 157

RDTR No. 157

/* EXEC FORTRAN

RDTR No. 157

TAPE OPERATING SYSTEM / 360 FORMAT 3,4-F5-439 2
SUBROUTINE HSC
COMMON T,TC,CC,EMIN,TW,MC,W,DK,MV,BT,VR,VBAR,CH,ALT,HL,H2,HC,HOPP
COMMON AREA1,AREA2,SUBT,V1,V2,G,PI,V,HASL,RC01(3),ARAR,R
COMMON K,IM1,LITER,FORMAT,IDL,ID2,IC3,NPROG,KODE
DOUBLE PRECISION T,TD
35 FORMAT(1HO,'OPTIMUM IGNITION ALTITUDE NOT FOUND')
36 FORMAT(1HI)
57 FORMAT(1HO,'OPTIMUM IGNITION ALTITUDE='',F11.0,2X,'',WMIN'',F5.3)
1. FEET')
WRITE(J,36)
H1=MOPP+BT*VBAR
H1=H1
HF=MOPP
H2=H1
SOB1=0.
SOB2=0.
SOBT=0.
INCM=(H1-HF)/10.**5
HINC=INCH
HIGH=H1
EXPNT=2./3.
2 1=0.
ABAR=0.
AREA1=0.
WT=TW
ALT=HIGH
CALL HEADER(5)
ARG=(CD*ALT/EMIN)**EXPNT-ALT*ALT
IF (ARG>16.16,17
16 R=0.
GO TO 18
17 A=SQR(T*ARG)
18 V=-SQR(TM/RHO)(ALT+HASL)/DK)
CALL HEADER(7)
AREA1=AREA2
7 DO 8 IT=1,LITER
CALL RALPH
IF (ALT>88.88,85
85 IF (LT-B1+.00C1) 87-.9,.89
8 V=V2
IF (ALT>88.88,89
88 ALT=0.
R=0.
CALL HEADER(7)
AREA1=AREA2
GO TO 9
9 ARG=(CD*ALT/EMIN)**EXPNT-ALT*ALT
IF (ARG>13.14
13 R=0.
GO TO 15
14 R=DQ(IARG)
15 CALL HEADER(7)
AREA1=AREA2
IF (LT-B1+.0001) 17,.9,9

RDTR No. 157

2002'

3000

RDTR No. 157

1500	CSO-10022
1501	CSO-10022
1502	CSO-10022
1503	CSO-10022
1504	CSO-10022
1505	CSO-10022
1506	CSO-10022
1507	CSO-10022
1508	CSO-10022
1509	CSO-10022
1510	CSO-10022
1511	CSO-10022
1512	CSO-10022
1513	CSO-10022
1514	CSO-10022
1515	CSO-10022
1516	CSO-10022
1517	CSO-10022
1518	CSO-10022
1519	CSO-10022
1520	CSO-10022
1521	CSO-10022
1522	CSO-10022
1523	CSO-10022
1524	CSO-10022
1525	CSO-10022
1526	CSO-10022
1527	CSO-10022
1528	CSO-10022
1529	CSO-10022
1530	CSO-10022
1531	CSO-10022
1532	CSO-10022
1533	CSO-10022
1534	CSO-10022
1535	CSO-10022
1536	CSO-10022
1537	CSO-10022
1538	CSO-10022
1539	CSO-10022
1540	CSO-10022
1541	CSO-10022
1542	CSO-10022
1543	CSO-10022
1544	CSO-10022
1545	CSO-10022
1546	CSO-10022
1547	CSO-10022
1548	CSO-10022
1549	CSO-10022
1550	CSO-10022
1551	CSO-10022
1552	CSO-10022
1553	CSO-10022
1554	CSO-10022
1555	CSO-10022
1556	CSO-10022
1557	CSO-10022
1558	CSO-10022
1559	CSO-10022
1560	CSO-10022
1561	CSO-10022
1562	CSO-10022
1563	CSO-10022
1564	CSO-10022
1565	CSO-10022
1566	CSO-10022
1567	CSO-10022
1568	CSO-10022
1569	CSO-10022
1570	CSO-10022
1571	CSO-10022
1572	CSO-10022
1573	CSO-10022
1574	CSO-10022
1575	CSO-10022
1576	CSO-10022
1577	CSO-10022
1578	CSO-10022
1579	CSO-10022
1580	CSO-10022
1581	CSO-10022
1582	CSO-10022
1583	CSO-10022
1584	CSO-10022
1585	CSO-10022
1586	CSO-10022
1587	CSO-10022
1588	CSO-10022
1589	CSO-10022
1590	CSO-10022
1591	CSO-10022
1592	CSO-10022
1593	CSO-10022
1594	CSO-10022
1595	CSO-10022
1596	CSO-10022
1597	CSO-10022
1598	CSO-10022
1599	CSO-10022
1600	CSO-10022

06/06/99

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0033

NON

SYMBOL	LOCATION	LOCATION
SYMBOL	LOCATION	LOCATION
T	0000	TD
WC	001C	W
BR	0030	VBAR
R2	0044	HC
SOBT	0058	V1
/	006C	HASL
C	0088	IM1
ID2	009C	ID3

LOCATION	SYMBOL	LOCATION	SYMBOL
0010	EMIN	0014	TW
0024	HV	0028	BT
0038	ALT	003C	H1
004C	AREA1	0050	AREA2
0060	G	0064	P1
0074	ABAR	0080	R
0090	KOMPUT	0094	1D1
00A4	KODE	00A8	

SCANNERS

LOCATION SYMBOL LOCATION SYMBOL LOCATION SYMBOL

LOCATION SYMBOL LOCATION SYMBOL

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LOCATION	LABEL	LOCATION	LABEL	LOCATION	LABEL	LOCATION	LABEL
000003	5	000017	5	000008	8	000009	9
000011	1	000018	2	000010	0	000010	0
000012	2	000019	0	000011	1	000011	1
000022	2	000020	0	000021	1	000021	1
02E8	8	000023	3	000024	4	000025	5
03A0	0	000026	6	000027	7	000028	8
044C	4	000028	8	000029	9	000029	9
046C	4	000030	0	000031	3	000032	2
049A	0	000033	3	000034	4	000035	5
0549A	5	000036	6	000037	7	000038	8
0549A	5	000039	9	000040	0	000041	1
0549A	5	000042	2	000043	3	000044	4
0549A	5	000045	5	000046	6	000047	7
0549A	5	000048	8	000049	9	000050	0
0549A	5	000051	1	000052	2	000053	3
0549A	5	000054	4	000055	5	000056	6
0549A	5	000057	7	000058	8	000059	9
0549A	5	000060	0	000061	1	000062	2
0549A	5	000063	3	000064	4	000065	5
0549A	5	000066	6	000067	7	000068	8
0549A	5	000069	9	000070	0	000071	1
0549A	5	000072	2	000073	3	000074	4
0549A	5	000075	5	000076	6	000077	7
0549A	5	000078	8	000079	9	000080	0
0549A	5	000081	1	000082	2	000083	3
0549A	5	000084	4	000085	5	000086	6
0549A	5	000087	7	000088	8	000089	9
0549A	5	000090	0	000091	1	000092	2
0549A	5	000093	3	000094	4	000095	5
0549A	5	000096	6	000097	7	000098	8
0549A	5	000099	9	000100	0	000101	1
0549A	5	000102	2	000103	3	000104	4
0549A	5	000105	5	000106	6	000107	7
0549A	5	000108	8	000109	9	000110	0
0549A	5	000111	1	000112	2	000113	3
0549A	5	000114	4	000115	5	000116	6
0549A	5	000117	7	000118	8	000119	9
0549A	5	000120	0	000121	1	000122	2
0549A	5	000123	3	000124	4	000125	5
0549A	5	000126	6	000127	7	000128	8
0549A	5	000129	9	000130	0	000131	1
0549A	5	000132	2	000133	3	000134	4
0549A	5	000135	5	000136	6	000137	7
0549A	5	000138	8	000139	9	000140	0
0549A	5	000141	1	000142	2	000143	3
0549A	5	000144	4	000145	5	000146	6
0549A	5	000147	7	000148	8	000149	9
0549A	5	000150	0	000151	1	000152	2
0549A	5	000153	3	000154	4	000155	5
0549A	5	000156	6	000157	7	000158	8
0549A	5	000159	9	000160	0	000161	1
0549A	5	000162	2	000163	3	000164	4
0549A	5	000165	5	000166	6	000167	7
0549A	5	000168	8	000169	9	000170	0
0549A	5	000171	1	000172	2	000173	3
0549A	5	000174	4	000175	5	000176	6
0549A	5	000177	7	000178	8	000179	9
0549A	5	000180	0	000181	1	000182	2
0549A	5	000183	3	000184	4	000185	5
0549A	5	000186	6	000187	7	000188	8
0549A	5	000189	9	000190	0	000191	1
0549A	5	000192	2	000193	3	000194	4
0549A	5	000195	5	000196	6	000197	7
0549A	5	000198	8	000199	9	000200	0
0549A	5	000201	1	000202	2	000203	3
0549A	5	000204	4	000205	5	000206	6
0549A	5	000207	7	000208	8	000209	9
0549A	5	000210	0	000211	1	000212	2
0549A	5	000213	3	000214	4	000215	5
0549A	5	000216	6	000217	7	000218	8
0549A	5	000219	9	000220	0	000221	1
0549A	5	000222	2	000223	3	000224	4
0549A	5	000225	5	000226	6	000227	7
0549A	5	000228	8	000229	9	000230	0
0549A	5	000231	1	000232	2	000233	3
0549A	5	000234	4	000235	5	000236	6
0549A	5	000237	7	000238	8	000239	9
0549A	5	000240	0	000241	1	000242	2
0549A	5	000243	3	000244	4	000245	5
0549A	5	000246	6	000247	7	000248	8
0549A	5	000249	9	000250	0	000251	1
0549A	5	000252	2	000253	3	000254	4
0549A	5	000255	5	000256	6	000257	7
0549A	5	000258	8	000259	9	000260	0
0549A	5	000261	1	000262	2	000263	3
0549A	5	000264	4	000265	5	000266	6
0549A	5	000267	7	000268	8	000269	9
0549A	5	000270	0	000271	1	000272	2
0549A	5	000273	3	000274	4	000275	5
0549A	5	000276	6	000277	7	000278	8
0549A	5	000279	9	000280	0	000281	1
0549A	5	000282	2	000283	3	000284	4
0549A	5	000285	5	000286	6	000287	7
0549A	5	000288	8	000289	9	000290	0
0549A	5	000291	1	000292	2	000293	3
0549A	5	000294	4	000295	5	000296	6
0549A	5	000297	7	000298	8	000299	9
0549A	5	000300	0	000301	1	000302	2
0549A	5	000303	3	000304	4	000305	5
0549A	5	000306	6	000307	7	000308	8
0549A	5	000309	9	000310	0	000311	1
0549A	5	000312	2	000313	3	000314	4
0549A	5	000315	5	000316	6	000317	7
0549A	5	000318	8	000319	9	000320	0
0549A	5	000321	1	000322	2	000323	3
0549A	5	000324	4	000325	5	000326	6
0549A	5	000327	7	000328	8	000329	9
0549A	5	000330	0	000331	1	000332	2
0549A	5	000333	3	000334	4	000335	5
0549A	5	000336	6	000337	7	000338	8
0549A	5	000339	9	000340	0	000341	1
0549A	5	000342	2	000343	3	000344	4
0549A	5	000345	5	000346	6	000347	7
0549A	5	000348	8	000349	9	000350	0
0549A	5	000351	1	000352	2	000353	3
0549A	5	000354	4	000355	5	000356	6
0549A	5	000357	7	000358	8	000359	9
0549A	5	000360	0	000361	1	000362	2
0549A	5	000363	3	000364	4	000365	5
0549A	5	000366	6	000367	7	000368	8
0549A	5	000369	9	000370	0	000371	1
0549A	5	000372	2	000373	3	000374	4
0549A	5	000375	5	000376	6	000377	7
0549A	5	000378	8	000379	9	000380	0
0549A	5	000381	1	000382	2	000383	3
0549A	5	000384	4	000385	5	000386	6
0549A	5	000387	7	000388	8	000389	9
0549A	5	000390	0	000391	1	000392	2
0549A	5	000393	3	000394	4	000395	5
0549A	5	000396	6	000397	7	000398	8
0549A	5	000399	9	000400	0	000401	1
0549A	5	000402	2	000403	3	000404	4
0549A	5	000405	5	000406	6	000407	7
0549A	5	000408	8	000409	9	000410	0
0549A	5	000411	1	000412	2	000413	3
0549A	5	000414	4	000415	5	000416	6
0549A	5	000417	7	000418	8	000419	9
0549A	5	000420	0	000421	1	000422	2
0549A	5	000423	3	000424	4	000425	5
0549A	5	000426	6	000427	7	000428	8
0549A	5	000429	9	000430	0	000431	1
0549A	5	000432	2	000433	3	000434	4
0549A	5	000435	5	000436	6	000437	7
0549A	5	000438	8	000439	9	000440	0
0549A	5	000441	1	000442	2	000443	3
0549A	5	000444	4	000445	5	000446	6
0549A	5	000447	7	000448	8	000449	9
0549A	5	000450	0	000451	1	000452	2
0549A	5	000453	3	000454	4	000455	5
0549A	5	000456	6	000457	7	000458	8
0549A	5	000459	9	000460	0	000461	1
0549A	5	000462	2	000463	3	000464	4
0549A	5	000465	5	000466	6	000467	7
0549A	5	000468	8	000469	9	000470	0
0549A	5	000471	1	000472	2	000473	3
0549A	5	000474	4	000475	5	000476	6
0549A	5	000477	7	000478	8	000479	9
0549A	5	000480	0	000481	1	000482	2
0549A	5	000483	3	000484	4	000485	5
0549A	5	000486	6	000487	7	000488	8
0549A	5	000489	9	000490	0	000491	1
0549A	5	000492	2	000493	3	000494	4
0549A	5	000495	5	000496	6	000497	7
0549A	5	000498	8	000499	9	000500	0
0549A	5	000501	1	000502	2	000503	3
0549A	5	000504	4	000505	5	000506	6
0549A	5	000507	7	000508	8	000509	9
0549A	5	000510	0	000511	1	000512	2
0549A	5	000513	3	000514	4	000515	5
0549A	5	000516	6	000517	7	000518</td	

10

LOCATION	LABEL
0210	00016
J2BC	00008
0372	00015
042E	00012
J4DD	00106

0522
ADDRESS BASE TABLE

RDTR No. 157

RDTR No. 157

// EXEC FORTRAN

ROTC No. 157

0002

```
06/06/69
ROOTS
43 IF(ROOT(1)-ROOT(2))47,46,46
47 R1=ROOT(1)
ROOT(1)=ROOT(2)
ROOT(2)=R1
46 K=1
RETURN
44 DO 48 I=1,N
E=CD*ROOT(1)/SQRT(ROOT(1)*ROOT(1)+ALT*ALT)**3
48 WRITE(3,49), ROOT(1), E, ALT
49 FORMAT(1.0, 'ROOT(1)', 11, 0)=', E15.6,5X, 'E=0, E15.6,5X, 'ALT='0, E15.6)
39 WRITE(3,41)P,PQ,Q
41 FORMAT(1.0, 'P= ', E15.6,5X, 'PQ= ', E15.6,5X, 'Q= ', E15.6/1
3 K=0
ROOT(1)=0.
ROOT(2)=0.
RETURN
END
```

RDTR No. 157

06/06/69

RDTSIS

0003

COMMON					
LOCATION	LOCATION	LOCATION	LOCATION	LOCATION	LOCATION
T 000	TD 0008	CD 0010	EMIN 0014	TW 0018	
WC 001C	W 0020	DK 0024	HV 0039	B 002C	
62 0030	VBAR 0034	DH 0038	ALT 0035	H1 004C	
H2 0044	HC 0048	HOP1 004C	AREA1 0050	AREA2 0054	
SOBT 0058	V1 005C	V2 0060	G 0064	P1 006E	
V 006C	HASL 0070	ROOT 0074	ABAR 0080	R 0084	
K 0088	I1 008C	ITER 0090	KOMPUT 0094	I01 0098	
ID2 009C	IC3 00A0	NPROG 00A4	KODE 00A8		
SCALARS					
CP 0110	H 0114	P 0118	PQ 0120	Q 0126	
A 0130	N 0138	COSA 013C	ALPHA 014J	R 0148	
I 014C	E				
CALLED SUBROUTINES					
IJTACOM DCCS	IJTADXD	IJTARXI	IJTSSQT	SORT	IJTLTAN
				DATAN	IJTLSQT
					DSQRT
					IJTLCN
LABEL	LOCATION	LOCATION	LOCATION	LABEL	LOCATION
00002	012C	C0013	019A	00017	01C4
00029	0248	0C018	027A	00021	03FC
00022	0462	00029	048C	00032	049C
00034	0500	00035	0526	00040	00043
00046	0590	00044	05AE	00048	0606
00041	0684	00003	060E	00049	0658
COMPILATION COMPLETE	AMOUNT OF COMMON	000172	AMOUNT OF CORE	002192	ADDRESS BASE TABLE
					06D0

RDTR No. 157

// EXEC FORTRAN

RDTR No. 157

0002

06/06/69 HEADER
CALL EXIT
16 WRITE(3,17)AREA2,RCCT(2),RCCT(1),T,ALT,V,SOBT,ABAK
RETURN
19 WRITE(3,18)AREA2,R,T,ALT,V,SOBT,ABAR
RETURN
ENC

04/06/69

HEADER

0003

COMMON					
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
T	0000	TD	0008	CD	0010
WC	001C	W	0020	DK	0024
BR	0030	VBAR	0034	DH	0038
H2	0044	HC	0048	HOPT	004C
S08T	0058	VI	005C	V2	006C
V	006C	MASL	0070	ROOT	0074
K	0088	IHL	008C	ITER	0090
ID2	009C	I03	00A0	NPROG	00A4
SCALARS					
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
N	NN	NN	00C4	CALLED SUBROUTINES	
LTTAAFR	LTTACOM	LTTFFIT	EXIT		
LABEL					
LABEL	LOCATION	LABEL	LOCATION	LABEL	LOCATION
00007	000E	00008	00A8	00009	00C2
00017	0110	00016	0131	00044	0160
00034	01CA	00035	01FA	00444	0256
00002	0352	00003	038A	00004	03C2
00012	04AA	00013	0524	00014	0582
00021	05CC	00022	05DE	00023	062E
COMPILEATION COMPLETE	AMOUNT OF COMMON 300172	AMOUNT OF CORE 002036	AMOUNT OF ADDRESS BASE TABLE 00019	AMOUNT OF CORE 002036	AMOUNT OF ADDRESS BASE TABLE 006FU

RDTR No. 157

// EXEC FORTRAN

RDTR No. 157

TAPE OPERATING SYSTEM/360 FORTRAN 360M-F0-409 20

```
FUNCTION RHO(H)
RHO=.07513*EXP(-3.1582E-5*H)
RETURN
END
```

06/06/69

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0002

SCALARS

SYMBOL	LOCATION	SYMBOL	LOCATION
RHO	004C	H	0048

CALLED SUBROUTINES

IJTACOM IJTEXPN- EXP

LABEL LOCATION LABEL LOCATION LABEL LOCATION
LOCATION COMMON 00000 AMOUNT OF CORE 000244 ADDRESS BASE TABLE 0088
COMPILATION COMPLETE

56

RDTR No. 157

RDTR No. 157

ii EXEC FORTRAN

TAPE OPERATING SYSTEM/360 FORTRAN 360M-F0-409 20

```
SUBROUTINE RALPH
COMMON T,TD,CD,EMIN,TW,WC,W,DK,HV,BT,BR,VBAR,DH,ALT,H1,H2,HC,HOPT
COMMON AREA1,AREA2,SOBT,V1,V2,G,PI,V,HASL,ROOT(3),ABAR,R
COMMON K,IH1,ITER,KOMPUT,IDL,IO2,IO3,NPROG,KODE
DOUBLE PRECISION T,TD
B=DK*RHO((ALT+HASL)*G/W
A1=-G*B*V*V
V1=V+TD*A1
A2=-G*B*V1*V1
V2=V+TD*((A1+A2)/2.)
ALT=ALT+TD*((V+V2)/2.)
T=T+TD
W=W-BR*TD
RETURN
END
```

RDTR No. 157

06/36/69

RALPH

0002

COMMON

SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
I	0000	ID	0008	CD	0010	EMIN	0014
MC	001C	W	0020	DK	0024	HV	0018
BR	0030	VBAR	0034	DH	0038	ALT	002C
H2	0044	HC	0048	HOPT	004C	AREA1	0040
SORT	0058	V1	005C	V2	0060	G	0054
V	006C	HASL	0070	ROOT	0074	ABAR	0068
K	0088	IHI	008C	ITER	0090	KOMPUR	0084
ID2	009C	I03	00A0	MPROG	00A4	KODE	0098

SCALARS

SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
B	004C	A1	0050	A2	0054		

CALLED SUBROUTINES

IJACOM RHO

LABEL LOCATION LABEL
COMPILATION COMPLETE AMOUNT OF COMMON 000172

LABEL LOCATION LABEL
AMOUNT OF CORE 000392 ADDRESS BASE TABLE 0116

RDTR No. 157

RDTR No. 157

// EXEC LNKEDT

JOB TE7P40 06/06/63 TAPE LINKAGE EDITOR DIAGNOSTIC OF INPUT

ACTION TAKEN	MAP
LIST	PHASE TE7P40,S
LIST	IJTAAFR
LIST	IJTAAINK
LIST	IJTACOM
LIST	IJTACOMK
LIST	IJTADXD
LIST	IJTAPST
LIST	IJTARX1
LIST	IJTARXK
LIST	IJTESPN
LIST	IJTFIOS
LIST	IJTFEXIT
LIST	IJTLEXP
LIST	IJTLLOG
LIST	IJTLCMN
LIST	IJTLSQT
LIST	IJTLTAN
LIST	IJTSLOG
LIST	IJTSSQT
LIST	ENTRY

RDTR No. 157

RDTR No. 157

06/26/69	PHASE	XFR-AD	LOCN#	HICHE	ES-17-	LABEL	LOCATED	REL-FP
COPMGN								
TE7P40		001080	00495F	CSECT	FCRTPAIN	JJ18B3	JJ18C9	000)AC
				CSECT	IJTAAFK	0J4578	0J4578	
				CSECT	IJTACCM	0J4618	0J4618	
				ENTPV	IJTSAVE	0J4828		
				CSECT	IJTFAIT	0J6128	0J6128	
				ENTRY	EXIT	JJ6128		
				CSECT	RHO	0J42F8	0J42F8	
				CSECT	IJTLSQT	0J6688	0J6688	
				ENTRY	DSQRT	00688E		
				CSECT	VSB1	0J1058	0J1058	
				CSECT	VSF1	0J2158	0J2158	
				CSECT	HSB1	0J2458	0J2458	
				CSECT	HSF1	0J2878	0J2878	
				CSECT	HSO	0J28C8	0J28C8	
				CSECT	HEADER	0J3802	0J3802	
				CSECT	ROOTS	0J3272	0J3272	
				CSECT	RALPH	0J43F0	0J43F0	
				CSECT	IJTARXR	0J5953	0J5953	
				CSECT	IJTAXD	0J5772	0J5772	
				CSECT	IJTARI	0J58C8	0J58C8	
				CSECT	IJTLIAN	0J6678	0J6678	
				ENTRY	DATAN	JU667E		
				CSFCT	IJTLSQT	0J65E8	0J65E8	
				ENTRY	DSQRT	0J65EE		
				CSECT	IJTLSCM	0J6478	0J6478	
				ENTRY	DCOS	JJ647E		
				*	ENTRY	DSIN	0J6498	
				CSECT	IJTEXPN	0J5A20	0J5A20	
				ENTRY	EXP	0J5A24		
				CSECT	IJTACON	0J4E28	0J4E28	
				*	ENTRY	FCVFI	0J4E28	

06/06/69

PHASE XFR-AD LOCORE HICORE ESD TYPE LABEL LOADED REL-FR

* ENTRY	FCVFO	004E2C
* ENTRY	FCVEI	004E30
* ENTRY	FCVEO	004E34
* ENTRY	FCVII	004E38
* ENTRY	FCVIO	004E3C
* ENTRY	FCVDI	004FDD
* ENTRY	FCVDC	0051CO
 CSECT	IJTFFIOS	005B38
ENTRY	UNITABE	006064
* ENTRY	D01XXE	005E72
* ENTRY	GETUNTE	005D84
* ENTRY	OPENUNE	005DU2
* ENTRY	SETLGUE	005E42
* ENTRY	CCWN01E	005F30
 CSECT	IJTapst	005B38
CSECT	IJTLLOG	006308
ENTRY	DLOG	006326
* ENTRY	DL0610	006310
 CSECT	IJTLXF	006140
ENTRY	DEXP	006146
 CSECT	IJTLXG	0067B0
ENTRY	ACJF	0067A2
* ENTRY	ACJL10	0067A8

TEPP4

P-5-58

RTN NO. 157

RDTR No. 157

// EXEC

RDTR No. 157

APPENDIX B

PROGRAM PRINTOUT

MK 45-8

CD
1.6530E .6EMIN
0.0200WC
17.50HC
5635.1BT
180.0TW
22.50

AREA	RADIUS2	RADIUS1	TIME	HEIGHT	VELOCITY	AREA-TIME INTEGRAL	AVERAGE AREA
2.44763E 08	64.	8827.	0.0	1740.	-10.032	0.0	0.0
2.46377E 08	54.	8856.	10.0	1641.	-9.803	2.45570E 09	2.45570E 08
2.47857E 08	45.	8882.	20.0	1544.	-9.554	4.92687E 09	2.46344E 08
2.49211E 08	37.	8907.	30.0	1449.	-9.321	7.41221E 09	2.47074E 08
2.50444E 08	31.	8929.	40.0	1358.	-9.073	9.91048E 09	2.4762E 08
2.51564E 08	25.	8949.	50.0	1268.	-8.820	1.24205E 10	2.48410E 08
2.52578E 08	20.	8967.	60.0	1181.	-8.562	1.49412E 10	2.49020E 08
2.53491E 08	16.	8983.	70.0	1097.	-8.297	1.74716E 10	2.49594E 08
2.54309E 08	13.	8997.	80.0	1015.	-8.026	2.09106E 10	2.50132E 08
2.55039E 08	11.	9010.	90.0	936.	-7.747	2.25573E 10	2.50637E 08
2.55686E 08	9.	9022.	100.0	860.	-7.459	2.51109E 10	2.51109E 08
2.56256E 08	7.	9032.	110.0	787.	-7.162	2.76706E 10	2.51551E 08
2.56755E 08	6.	9040.	120.0	717.	-6.853	3.02357E 10	2.51964E 08
2.57187E 08	5.	9048.	130.0	650.	-6.532	3.28054E 10	2.52349E 08
2.57559E 08	5.	9054.	140.0	586.	-6.195	3.53791E 10	2.52708E 08
2.57875E 08	4.	9060.	150.0	526.	-5.842	3.79563E 10	2.53042E 08
2.58141E 08	4.	9065.	160.0	470.	-5.467	4.05364E 10	2.53352E 08
2.58362E 08	4.	9069.	170.0	417.	-5.067	4.31189E 10	2.53640E 08
2.58542E 08	4.	9072.	180.0	368.	-4.639	4.57034E 10	2.53908E 08

RDTR No. 157

PK 45-8		VSB		TW		WC		HASL		AVERAGE AREA	
CD	EMIN	HC	BT	TW	WC	HC	BT	HASL	0.	0.	0.
1.6500E 06	0.0200	5635.1	180.0	22.50	17.50	DK	3.14382				
AREA	RADIUS2	RADIUS1	TIME	HEIGHT	VELOCITY	AREA-TIME INTEGRAL					
2.45880E 08	57.	8847.	0.0	1672.	-10.021	0.0					
2.47425E 08	47.	8875.	10.3	1573.	-9.792	2.46652E 09					
2.48838E 08	39.	8900.	20.0	1476.	-9.554	4.94783E 09					
2.50126E 08	32.	8923.	30.0	1382.	-9.311	7.44265E 09					
2.51298E 08	26.	8944.	40.0	1290.	-9.064	9.94977E 09					
2.52358E 08	21.	8963.	50.0	1201.	-8.811	1.24680E 10					
2.53313E 08	17.	8980.	60.0	1114.	-8.553	1.49964E 10					
2.54170E 08	14.	8995.	70.0	1029.	-8.288	1.75338E 10					
2.54935E 08	11.	9008.	80.0	948.	-8.017	2.00793E 10					
2.55613E 08	9.	9020.	90.0	869.	-7.739	2.26321E 10					
2.56211E 08	7.	9031.	100.0	793.	-7.451	2.51912E 10					
2.56734E 08	6.	9040.	110.0	720.	-7.154	2.77559E 10					
2.57187E 08	5.	9048.	120.0	650.	-6.846	3.03255E 10					
2.57577E 08	5.	9055.	130.0	583.	-6.525	3.28993E 10					
2.57908E 08	4.	9061.	140.0	520.	-6.189	3.54767E 10					
2.58186E 08	4.	9065.	150.0	459.	-5.836	3.80572E 10					
2.58416E 08	4.	9070.	160.0	403.	-5.461	4.06402E 10					
2.58603E 08	4.	9073.	170.0	350.	-5.061	4.32253E 10					
2.58752E 08	4.	9075.	180.0	302.	-4.634	4.58121E 10					

MK 45-8

CD	EMIN	TW	WC
1.6503E 06	0.0200	22.50	17.50

HC	BT	DK	HASL
5635.1	180.0	3.14382	0.

AREA	RADIUS2	RADIUS1	TIME	HEIGHT	VELOCITY	AREA-TIME INTEGRAL	AVERAGE AREA
2.45912E 08	57.	8848.	0.0	1670.	-10.021	0.0	0.0
2.47455E 08	47.	8875.	10.0	1571.	-9.792	2.46684E 09	2.46684E 08
2.48866E 08	39.	8900.	20.0	1474.	-9.553	4.94843E 09	2.47422E 08
2.50153E 08	32.	8923.	30.0	1380.	-9.311	7.44353E 09	2.48118E 08
2.51322E 08	26.	8944.	40.0	1288.	-9.063	9.95090E 09	2.48772E 08
2.52380E 08	21.	8963.	50.0	1199.	-8.811	1.24694E 10	2.49388E 08
2.53334E 08	17.	8980.	60.0	1112.	-8.553	1.49980E 10	2.49966E 08
2.54190E 08	14.	8995.	70.0	1027.	-8.288	1.75356E 10	2.50508E 08
2.54953E 08	11.	9009.	80.0	946.	-8.017	2.00813E 10	2.51016E 08
2.55629E 08	9.	9021.	90.0	867.	-7.738	2.26342E 10	2.51491E 08
2.56226E 08	7.	9031.	100.0	791.	-7.451	2.51935E 10	2.51935E 08
2.56747E 08	6.	9040.	110.0	718.	-7.154	2.77583E 10	2.52348E 08
2.57199E 08	5.	9048.	120.0	648.	-6.846	3.03281E 10	2.52734E 08
2.57587E 08	5.	9055.	130.0	581.	-6.525	3.29020E 10	2.53092E 08
2.57917E 08	4.	9061.	140.0	518.	-6.189	3.54795E 10	2.53425E 08
2.58194E 08	4.	9066.	150.0	457.	-5.835	3.80601E 10	2.53734E 08
2.58423E 08	4.	9070.	160.0	401.	-5.461	4.06432E 10	2.54020E 08
2.58609E 08	4.	9073.	170.0	348.	-5.061	4.32283E 10	2.54284E 08
2.58757E 08	4.	9076.	180.0	300.	-4.634	4.58151E 10	2.54529E 08

MK 45-8

HSB

CD	E ^{MIN}	TW	WC
1.6500E-06	0.0230	22.50	17.50
OPT. ALT.	BT	DK	HASL
3984.6	180.0	3.14382	0.

AREA	RADIUS	TIME	HEIGHT	VELOCITY	AREA-TIME INTEGRAL	AVERAGE AREA
7.50407E 07	4887.	0.0	1670.	-10.021	0.0	0.0
7.27006E 07	4811.	10.0	1571.	-9.792	7.38706E 08	7.38706E 07
7.02882E 07	4730.	20.0	1474.	-9.553	7.26825E 07	7.26825E 07
6.78084E 07	4646.	30.0	1380.	-9.311	7.14711E 07	7.14711E 07
6.52650E 07	4558.	40.0	1288.	-9.063	7-J2375E 07	7.02950E 09
6.26631E 07	4466.	50.0	1199.	-8.811	6.89828E 07	3.44914E 09
6.00081E 07	4370.	60.0	1112.	-8.553	6.77083E 07	4.06250E 09
5.73051E 07	4271.	70.0	1027.	-8.288	6.64906E 09	6.64151E 07
5.45599E 07	4167.	80.0	946.	-8.017	6.51047E 07	5.20338E 09
5.17768E 07	4060.	90.0	867.	-7.738	6.37784E 07	5.74036E 09
4.89624E 07	3948.	100.0	791.	-7.451	6.24375E 07	6.24375E 09
4.61239E 07	3832.	110.0	718.	-7.154	6.10835E 07	6.71918E 09
4.32684E 07	3711.	120.0	648.	-6.846	5.97179E 07	7.16614E 09
4.04036E 07	3586.	130.0	581.	-6.525	5.83423E 07	7.58450E 09
3.75410E 07	3457.	140.0	518.	-6.189	5.69587E 07	7.97422E 09
3.46910E 07	3323.	150.0	457.	-5.835	5.55692E 07	8.33528E 09
3.18687E 07	3185.	160.0	401.	-5.461	5.41761E 07	8.66818E 09
2.90933E 07	3043.	170.0	348.	-5.061	5.27823E 07	8.97298E 09
2.63887E 07	2898.	180.0	300.	-4.634	5.13911E 07	9.25039E 09

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MK 45-8		VS8		NC		TW		EMIN		CD	
AREA	RADIUS2	RADIUS1	TIME	HEIGHT	VELOCITY	AREA-TIME INTEGRAL	HASL	TW	0.0500	HC	3563.9
9.01519E 07	143.	5359.	0.0	1670.	-10.021	0.0	0.	22.50	17.50		
9.17574E 07	119.	5406.	10.0	1571.	-9.792	9.39546E 08				9.09546E 07	
9.32166E 07	98.	5448.	20.0	1474.	-9.553	1.83442E 09				9.17208E 07	
9.45400E 07	80.	5486.	30.0	1380.	-9.311	2.77320E 09				9.24400E 07	
9.57370E 07	65.	5521.	40.0	1288.	-9.063	3.72458E 09				9.31146E 07	
9.68161E 07	52.	5552.	50.0	1193.	-8.811	4.68735E 09				9.37469E 07	
9.77855E 07	42.	5579.	60.0	1112.	-8.553	5.66035E 09				9.43392E 07	
9.86524E 07	33.	5604.	70.0	1027.	-8.288	6.64254E 09				9.48934E 07	
9.94240E 07	26.	5626.	80.0	946.	-8.017	7.63292E 09				9.54115E 07	
1.00107E 08	20.	5645.	90.0	867.	-7.738	8.63058E 09				9.58952E 07	
1.00708E 08	15.	5662.	100.0	791.	-7.451	9.63464E 09				9.63464E 07	
1.01232E 08	11.	5677.	110.0	718.	-7.154	1.06443E 10				9.67667E 07	
1.01686E 08	9.	5689.	120.0	648.	-6.846	1.16589E 10				9.71578E 07	
1.02076E 08	6.	5700.	130.0	581.	-6.525	1.26777E 10				9.75211E 07	
1.02407E 08	5.	5709.	140.0	516.	-6.189	1.37002E 10				9.78583E 07	
1.02684E 08	4.	5717.	150.0	457.	-5.835	1.47256E 10				9.81707E 07	
1.02914E 08	3.	5724.	160.0	401.	-5.461	1.57536E 10				9.84600E 07	
1.03100E 08	3.	5729.	170.0	348.	-5.061	1.67837E 10				9.87274E 07	
1.03248E 08	3.	5733.	180.0	300.	-4.634	1.78154E 10				9.89745E 07	

MK 45-8		HSSB		TW		WC	
CD	EMIN	CD	EMIN	DK	HASL	CD	WC
1.6500E 06	0.0500	180.0	180.0	22.50	3.14382	17.50	
OPT. ALT.	BT						
2520.1							
AREA	RADIUS	TIME	HEIGHT	VELOCITY	AREA-TIME INTEGRAL	AREA	AVERAGE AREA
3.67336E 07	3419.	0.0	1670.	-10.021	0.0	0.0	0.0
3.59244E 07	3382.	10.0	1571.	-9.792	3.63290E 08	3.63290E 07	
3.50378E 07	3340.	20.0	1474.	-9.553	7.18101E 08	3.59050E 07	
3.40776E 07	3294.	30.0	1380.	-9.311	1.06368E 09	3.54559E 07	
3.30494E 07	3242.	40.0	1288.	-9.063	1.39931E 09	3.49828E 07	
3.19561E 07	3189.	50.0	1199.	-8.811	1.72434E 09	3.44868E 07	
3.08028E 07	3131.	60.0	1112.	-8.553	2.03813E 09	3.39689E 07	
2.95941E 07	3069.	70.0	1027.	-8.288	2.34012E 09	3.34303E 07	
2.83344E 07	3003.	80.0	946.	-8.017	2.62976E 09	3.28720E 07	
2.70287E 07	2933.	90.0	867.	-7.738	2.90658E 09	3.22953E 07	
2.56820E 07	2859.	100.0	791.	-7.451	3.17013E 09	3.17013E 07	
2.42994E 07	2781.	110.0	718.	-7.154	3.42094E 09	3.10912E 07	
2.28866E 07	2699.	120.0	648.	-6.846	3.65597E 09	3.04664E 07	
2.14495E 07	2613.	130.0	581.	-6.525	3.87765E 09	2.98280E 07	
1.99957E 07	2523.	140.0	518.	-6.189	4.08487E 09	2.91776E 07	
1.85328E 07	2429.	150.0	457.	-5.835	4.27752E 09	2.85168E 07	
1.70703E 07	2331.	160.0	401.	-5.461	4.45553E 09	2.78471E 07	
1.56201E 07	2230.	170.0	348.	-5.061	4.61898E 09	2.71705E 07	
1.41969E 07	2126.	180.0	300.	-4.634	4.76806E 09	2.64892E 07	

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MK 45-8		VSB		WC		AVERAGE AREA	
CD	EMIN	TW	DK	HASL	0.	0.	0.
1.6500E .96	0.1033	BT					
HC	2520.1	180.0					
AREA	RADIUS2	RADIUS1	TIME	HEIGHT	VELOCITY	AREA-TIME INTEGRAL	AVERAGE AREA
3.76879E 07	296.	3476.	0.3	1670.	-10.021	0.0	0.0
3.94702E 07	243.	3553.	10.0	1571.	-9.792	3.85790E 08	3.85790E 07
4.10572E 07	200.	3621.	20.0	1474.	-9.553	7.88427E 08	3.94213E 07
4.24732E 07	163.	3680.	30.0	1380.	-9.311	1.23608E 09	4.02026E 07
4.37371E 07	132.	3734.	40.0	1288.	-9.063	1.63713E 09	4.09283E 07
4.48645E 07	106.	3780.	50.0	1199.	-8.811	2.08014E 09	4.16028E 07
4.58686E 07	84.	3822.	60.0	1112.	-8.553	2.53380E 09	4.22309E 07
4.67603E 07	66.	3859.	70.0	1027.	-8.288	2.99695E 09	4.28135E 07
4.75495E 07	52.	3891.	80.0	946.	-8.017	3.46850E 09	4.33562E 07
4.82448E 07	40.	3919.	90.0	867.	-7.738	3.94747E 09	4.38608E 07
4.88541E 07	30.	3944.	100.0	791.	-7.451	4.43296E 09	4.43296E 07
4.93846E 07	23.	3965.	110.0	718.	-7.154	4.92415E 09	4.47650E 07
4.98429E 07	17.	3983.	120.0	648.	-6.846	5.42029E 09	4.51691E 07
5.02354E 07	12.	3999.	130.0	561.	-6.525	5.92068E 09	4.55437E 07
5.05681E 07	9.	4012.	140.0	518.	-6.189	6.42469E 09	4.58907E 07
5.08466E 07	6.	4023.	150.0	457.	-5.835	6.93177E 09	4.62118E 07
5.10767E 07	4.	4032.	160.0	401.	-5.461	7.44138E 09	4.65086E 07
5.12634E 07	3.	4040.	170.0	348.	-5.061	7.95308E 09	4.67828E 07
5.14120E 07	2.	4045.	180.0	300.	-4.634	8.46646E 09	4.70359E 07

MK - 5-8		HSB		WC 17.50		TW 22.50		DK 3.14382		HASL 0.		AREA-TIME INTEGRAL		AVERAGE AREA						
L.D	EMIN	L.D	EMIN	OPT. ALT.	BT	OPT. ALT.	BT	RADIUS	TIME	HEIGHT	VELOCITY	OPT. ALT.	BT	RADIUS	TIME	HEIGHT	VELOCITY	OPT. ALT.	BT	
1.6500E 06	0.1000	1.6500E 06	0.1000	1782.0	180.0	1782.0	180.0	2517.	0.0	1670.	-10.021	0.0	0.0	0.0	0.0	0.0	1.98305E 08	1.98305E 07		
1.97625E 07	27	2508.	10.0	1571.	-9.792	1.97424E 07	27	2494.	20.0	1474.	-9.553	3.94849E 08	1.97424E 07	2476.	30.0	1380.	-9.311	5.88853E 08	1.96284E 07	
1.95463E 07	07	2424.	50.0	1199.	-8.811	1.93273E 07	07	2392.	60.0	1112.	-8.553	1.14849E 09	1.91416E 07	2452.	40.0	1288.	-9.063	7.79584E 08	1.94896E 07	
1.8816E 07	07	2355.	70.0	1027.	-8.288	1.89345E 07	07	2313.	80.0	946.	-8.017	1.49654E 09	1.87068E 07	2268.	90.0	867.	-7.738	1.66136E 09	1.84595E 07	
1.79680E 07	07	2221.	100.0	791.	-7.451	1.81938E 09	07	2164.	110.0	718.	-7.154	1.97173E 09	1.79107E 07	2106.	120.0	648.	-6.846	2.11336E 09	1.76113E 07	
1.74160E 07	07	2044.	130.0	581.	-6.525	2.24860E 09	07	1.39292E 07	1908.	457.	-5.835	2.49421E 09	1.66281E 07	1.31196E 07	1977.	140.0	518.	-6.189	2.37563E 09	1.69688E 07
1.22850E 07	07	1908.	150.0	401.	-5.461	2.60420E 09	07	1.14317E 07	1834.	160.0	-5.061	2.79553E 09	1.62763E 07	1.05667E 07	1834.	170.0	348.	-4.634	2.79822E 09	1.59149E 07
9.69899E 06	06	1757.	170.0	300.	-4.634	1.55457E 07	06	8.83899E 06	1677.	180.0	-4.634	2.79822E 09	1.55457E 07							

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CD		EMIN		HSO		TW		WC		AVERAGE AREA	
OPT.	ALI.	BT	180.0	OK	3.14382	HASL	0.	0.	17.50	0.0	
9.13559E	07	5393.	0.0	5425.	-10.633	0.0	0.0	9.19437E	08	9.19436E	07
9.25275E	07	5427.	10.0	5319.	-10.389	1.85000E	09	9.24998E	07	9.30201E	07
9.35845E	07	5458.	20.0	5216.	-10.135	2.79060E	09	9.35059E	07	9.39586E	07
9.45337E	07	5486.	30.0	5116.	-9.877	3.74024E	09	9.43794E	07	9.47693E	07
9.53896E	07	5510.	40.0	5019.	-9.613	4.69793E	09	9.63385E	09	9.51297E	07
9.61497E	07	5532.	50.0	4924.	-9.345	5.66277E	09	9.54620E	07	9.57675E	07
9.68170E	07	5551.	60.0	4831.	-9.070	6.63385E	09	9.63385E	09	9.63038E	09
9.74008E	07	5568.	70.0	4742.	-8.789	7.61038E	09	9.69382E	07	9.69382E	07
9.79047E	07	5582.	80.0	4655.	-8.501	8.59158E	09	9.71102E	07	9.72646E	07
9.83356E	07	5595.	90.0	4571.	-8.205	9.57675E	09	9.74029E	07	9.74029E	07
9.86984E	07	5605.	100.0	4491.	-7.899	1.05652E	10	9.77102E	07	9.77102E	07
9.89962E	07	5614.	110.0	4413.	-7.584	1.15564E	10	9.80322E	07	9.80322E	07
9.92363E	07	5620.	120.0	4339.	-7.256	1.25497E	10	9.85359E	07	9.85359E	07
9.94228E	07	5626.	130.0	4268.	-6.916	1.35446E	10	9.90472E	07	9.90472E	07
9.95637E	07	5630.	140.0	4200.	-6.559	1.45407E	10	9.95376E	07	9.95376E	07
9.96614E	07	5632.	150.0	4136.	-6.184	1.65350E	10	9.99382E	07	9.99382E	07
9.97210E	07	5634.	160.0	4076.	-5.787	1.65350E	10	9.997508E	07	9.997508E	07
9.97508E	07	5635.	170.0	4020.	-5.363	1.75325E	10	9.997551E	07	9.997551E	07
					-4.909						

PK 45-8		HSC		AVERAGE AREA	
CL	EMIN	TC	TW	DK	HASL
1.6500	.06	0.0200	22.50		17.50
OPT. ALT.		BT			
3984.6		180.0			
AREA	RADIUS	TIME	HEIGHT	VELOCITY	AREA-TIME INTEGRAL
9.29339E 07	5439.	0.0	5281.	-10.609	0.0
9.39837E 07	5470.	10.0	5176.	-10.366	9.34588E 08
9.49270E 07	5497.	20.0	5073.	-10.112	1.87914E 09
9.57632E 07	5521.	30.0	4973.	-9.854	2.83259E 09
9.65060E 07	5542.	40.0	4875.	-9.592	3.79394E 09
9.71546E 07	5561.	50.0	4781.	-9.324	4.76224E 09
9.77188E 07	5577.	60.0	4689.	-9.050	5.73660E 09
9.82001E 07	5591.	70.0	4599.	-8.769	6.71619E 09
9.86030E 07	5602.	80.0	4513.	-8.482	7.70021E 09
9.89379E 07	5612.	90.0	4429.	-8.186	8.68791E 09
9.92060E 07	5619.	100.0	4349.	-7.882	9.67863E 09
9.94146E 07	5625.	110.0	4271.	-7.567	1.06717E 10
9.95686E 07	5630.	120.0	4197.	-7.240	1.16666E 10
9.96718E 07	5633.	130.0	4126.	-6.900	1.26628E 10
9.97343E 07	5634.	140.0	4059.	-6.545	1.36599E 10
9.97571E 07	5635.	150.0	3995.	-6.171	1.46573E 10
9.97461E 07	5635.	160.0	3935.	-5.774	1.56548E 10
9.97112E 07	5634.	170.0	3880.	-5.351	1.66521E 10
9.96552E 07	5632.	180.0	3829.	-4.899	1.76490E 10

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MK 45-8		HSO		W.C.		AVERAGE AREA	
CD	EPIN	TW	DK	HASL	0.	0.0	
1.6500E 06	0.0200	22.50					
OPT. ALT.	BT						
3984.6	180.0		3.14382	0.			
AREA	RADIUS	TIME	HEIGHT	VELOCITY	AREA-TIME INTEGRAL		
9.43693E 07	5480.	0.0	5137.	-10.585	0.0		
9.52813E 07	5507.	10.0	5032.	-10.342	9.48153E 08		
9.61054E 07	5531.	20.0	4929.	-10.089	1.90509E 09		
9.68288E 07	5552.	30.0	4830.	-9.832	2.86976E 09		
9.74599E 07	5570.	40.0	4732.	-9.570	3.84120E 09		
9.80001E 07	5585.	50.0	4638.	-9.303	4.81850E 09		
9.84571E 07	5598.	60.0	4546.	-9.029	5.80978E 09		
9.88348E 07	5609.	70.0	4457.	-8.750	6.78724E 09		
9.91394E 07	5618.	80.0	4371.	-8.463	7.77711E 09		
9.93775E 07	5624.	90.0	4287.	-8.168	8.76969E 09		
9.95515E 07	5629.	100.0	4207.	-7.864	9.76434E 09		
9.96696E 07	5633.	110.0	4130.	-7.550	1.07604E 10		
9.97355E 07	5634.	120.0	4056.	-7.224	1.17575E 10		
9.97565E 07	5635.	130.0	3985.	-6.885	1.27549E 10		
9.97377E 07	5634.	140.0	3918.	-6.530	1.37524E 10		
9.96841E 07	5633.	150.0	3854.	-6.157	1.47495E 10		
9.96062E 07	5631.	160.0	3795.	-5.762	1.57459E 10		
9.95046E 07	5628.	170.0	3739.	-5.339	1.67415E 10		
9.93868E 07	5625.	180.0	3688.	-4.888	1.77360E 10		

RDTR No. 157

MK 45-8		MSO		TW		WC	
CC	EMIN	BT	DK	HASL	0.		
1.6530E 07	0.0200		22.50			17.50	
OPT. ALT.							
3984.6		180.0					
			3.14382				
AREA	RADIUS	TIME	HEIGHT	VELOCITY	AREA-TIME INTEGRAL	AVERAGE AREA	
9.56044E 07	5517.	0.0	4993.	-10.561	0.0	0.0	
9.64146E 07	5540.	10.0	4888.	-10.319	9.60095E 08	9.60095E 07	
9.71201E 07	5560.	20.0	4786.	-10.066	1.92777E 09	9.63884E 07	
9.77317E 07	5578.	30.0	4686.	-9.810	2.90203E 09	9.67343E 07	
9.82489E 07	5592.	40.0	4589.	-9.548	3.88193E 09	9.70483E 07	
9.86793E 07	5605.	50.0	4495.	-9.282	4.86657E 09	9.73314E 07	
9.90300E 07	5614.	60.0	4403.	-9.009	5.85511E 09	9.75852E 07	
9.93048E 07	5622.	70.0	4314.	-8.730	6.84678E 09	9.78112E 07	
9.95102E 07	5628.	80.0	4228.	-8.444	7.84086E 09	9.80107E 07	
9.96498E 07	5632.	90.0	4145.	-8.150	8.83666E 09	9.61951E 07	
9.97294E 07	5634.	100.0	4065.	-7.846	9.83355E 09	9.83355E 07	
9.97579E 07	5635.	110.0	3988.	-7.533	1.08310E 10	9.84635E 07	
9.97355E 07	5634.	120.0	3914.	-7.208	1.18284E 10	9.85704E 07	
9.96733E 07	5633.	130.0	3844.	-6.870	1.28255E 10	9.86576E 07	
9.95764E 07	5630.	140.0	3777.	-6.516	1.38217E 10	9.87267E 07	
9.94475E 07	5626.	150.0	3714.	-6.143	1.48169E 10	9.87790E 07	
9.92948E 07	5622.	160.0	3654.	-5.749	1.58106E 10	9.88160E 07	
9.91272E 07	5617.	170.0	3599.	-5.328	1.68027E 10	9.88392E 07	
9.89484E 07	5612.	180.0	3548.	-4.877	1.77930E 10	9.88503E 07	

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MK 45-8		HSO		AVERAGE AREA	
CD	EMIN	TW	WC	CD	CD
1.6500E 06	0.0200	22.50	17.50	9.70421E 07	9.70421E 07
CPT. ALT.	BT			9.73614E 07	9.73614E 07
3984.6	180.0	DK	HASL	9.76483E 07	9.76483E 07
		3.14382	0.	9.79043E 07	9.79043E 07
AREA	TIME	HEIGHT	VELOCITY	AREA-TIME INTEGRAL	AVERAGE AREA
9.66978E 07	5548.	0.0	4849.	-10.537	0.0
9.73865E 07	5568.	10.0	4744.	-10.295	9.70422E 08
9.79747E 07	5584.	20.0	4642.	-10.044	1.94723E 09
9.84698E 07	5599.	30.0	4543.	-9.788	2.92945E 09
9.88748E 07	5610.	40.0	4446.	-9.527	3.91617E 09
9.91965E 07	5619.	50.0	4352.	-9.261	4.90653E 09
9.94394E 07	5626.	60.0	4261.	-8.989	5.89971E 09
9.96104E 07	5631.	70.0	4172.	-8.710	6.89495E 09
9.97146E 07	5634.	80.0	4086.	-8.425	7.89157E 09
9.97549E 07	5635.	90.0	4003.	-8.131	8.88892E 09
9.97406E 07	5635.	100.0	3923.	-7.829	9.88640E 09
9.96766E 07	5633.	110.0	3847.	-7.516	1.08835E 10
9.95673E 07	5630.	120.0	3773.	-7.192	1.18797E 10
9.94210E 07	5626.	130.0	3703.	-6.854	1.28746E 10
9.92431E 07	5621.	140.0	3636.	-6.501	1.38680E 10
9.90382E 07	5615.	150.0	3573.	-6.130	1.48594E 10
9.08143E 07	5608.	160.0	3514.	-5.736	1.58486E 10
9.85781E 07	5602.	170.0	3458.	-5.316	1.68356E 10
9.83369E 07	5595.	180.0	3407.	-4.866	1.78202E 10

MK 45-8

HSD

CC
1.6500F 06
EMIN
0.0200

TW
WC
22.50
17.50

OPT. ALT.
3984.6
BT
180.0

AREA	RADIUS	TIME	HEIGHT	VELOCITY	AREA-TIME INTEGRAL	AVERAGE AREA
9.76238E 07	5574.	0.0	4705.	-10.513	0.0	0.0
9.81925E 07	5591.	10.0	4600.	-10.272	9.79081E 08	9.79081E 07
9.86640E 07	5604.	20.0	4499.	-10.021	1.96336E 09	9.81682E 07
9.90421E 07	5615.	30.0	4400.	-9.766	2.95189E 09	9.83965E 07
9.33354E 07	5623.	40.0	4303.	-9.505	3.94378E 09	9.85945E 07
9.95474E 07	5629.	50.0	4209.	-9.240	4.93819E 09	9.87639E 07
9.96820E 07	5633.	60.0	4118.	-8.968	5.93434E 09	9.89056E 07
9.97493E 07	5635.	70.0	4030.	-8.691	6.93149E 09	9.90213E 07
9.97488E 07	5635.	80.0	3944.	-8.406	7.92898E 09	9.91122E 07
9.96939E 07	5633.	90.0	3861.	-8.113	8.92619E 09	9.91799E 07
9.95834E 07	5630.	100.0	3782.	-7.811	9.92258E 09	9.92258E 07
9.94287E 07	5626.	110.0	3705.	-7.499	1.09176E 10	9.92512E 07
9.92299E 07	5620.	120.0	3632.	-7.176	1.19109E 10	9.92577E 07
9.89994E 07	5614.	130.0	3562.	-6.839	1.29021E 10	9.94467E 07
9.87379E 07	5606.	140.0	3495.	-6.487	1.38908E 10	9.92197E 07
9.84566E 07	5598.	150.0	3432.	-6.116	1.48767E 10	9.91782E 07
9.81589E 07	5590.	160.0	3373.	-5.723	1.58598E 10	9.91238E 07
9.78555E 07	5581.	170.0	3318.	-5.304	1.68399E 10	9.90581E 07
9.75518E 07	5572.	180.0	3267.	-4.855	1.78169E 10	9.89828E 07

MK 45-8		HSO			
CC	E _{MIN}	T _W	WC		
1.65COE 06	0.0200	22.50	17.50		
OPT. ALT.	BT	DK	HASL		
3984.6	180.0	3.14382	0.		
AREA	TIME	HEIGHT	VELOCITY	AREA-TIME INTEGRAL	AVERAGE AREA
5554.	0.0	4820.	-10.532	0.0	0.0
5573.	10.0	4715.	-10.290	9.72296E 38	9.72296E 37
5589.	20.0	4613.	-10.039	1.95073E 09	9.75367E 37
5602.	30.0	4514.	-9.783	2.93435E 09	9.78118E 07
5613.	40.0	4417.	-9.523	3.92225E 09	9.80561E 07
5622.	50.0	4323.	-9.257	4.91355E 09	9.82710E 07
5628.	60.0	4232.	-8.985	5.90746E 09	9.84517E 07
5632.	70.0	4143.	-8.706	6.90323E 09	9.86176E 07
5634.	80.0	4057.	-8.421	7.90016E 09	9.87519E 07
5635.	90.0	3975.	-8.128	8.89761E 09	9.88623E 07
5634.	100.0	3895.	-7.825	9.89499E 09	9.89499E 07
5632.	110.0	3818.	-7.513	1.08918E 10	9.90164E 07
5628.	120.0	3745.	-7.189	1.18876E 10	9.90632E 07
5624.	130.0	3674.	-6.851	1.28819E 10	9.90916E 07
5618.	140.0	3608.	-6.498	1.38744E 10	9.91032E 07
5612.	150.0	3545.	-6.127	1.48649E 10	9.90993E 07
5605.	160.0	3485.	-5.734	1.58531E 10	9.90816E 07
5598.	170.0	3430.	-5.313	1.68388E 10	9.90516E 07
5591.	180.0	3379.	-4.864	1.78220E 10	9.90108E 07

MK 45-6		MSD		TW		WC	
CD	E MIN	CD	E MIN	TW	WC	TW	WC
1.65E 06	0.0230	1.65E 06	0.0230	22.50	17.50	DK	HASL
OPT. ALT.	81	OPT. ALT.	81	3.14382	0.	DK	HASL
3984.6	180.0	3984.6	180.0	3.14382	0.	DK	HASL
AREA	RADIUS	TIME	HEIGHT	VELOCITY	AREA-TIME INTEGRAL	AREA	AREA
9.70908E 07	55559.	0.0	4791.	-10.527	0.0	0.0	0.0
9.77305E 07	55578.	10.0	46886.	-10.286	9.74106E 08	9.74106E 08	9.74106E 08
9.82712E 07	55593.	20.0	45855.	-10.034	1.95411E 09	9.77057E 07	9.77057E 07
9.87203E 07	56066.	30.0	44855.	-9.779	2.93907E 09	9.79691E 07	9.79691E 07
9.90804E 07	56166.	40.0	43899.	-9.518	3.92808E 09	9.82019E 07	9.82019E 07
9.93590E 07	5624.	50.0	4295.	-9.252	4.92027E 09	9.84054E 07	9.84054E 07
9.95580E 07	5629.	60.0	4203.	-8.981	5.91485E 09	9.85809E 07	9.85809E 07
9.96863E 07	5633.	70.0	4115.	-8.702	6.91107E 09	9.87296E 07	9.87296E 07
9.97488E 07	5635.	80.0	4029.	-8.417	7.90825E 09	9.88531E 07	9.88531E 07
9.97518E 07	5635.	90.0	3946.	-8.124	8.90575E 09	9.89528E 07	9.89528E 07
9.96994E 07	5633.	100.0	3866.	-7.822	9.90300E 09	9.90300E 07	9.90300E 07
9.95963E 07	5630.	110.0	3790.	-7.510	1.08995E 10	9.90861E 07	9.90861E 07
9.94516E 07	5626.	120.0	3716.	-7.186	1.19947E 10	9.91226E 07	9.91226E 07
9.92732E 07	5621.	130.0	3646.	-6.848	1.28883E 10	9.91411E 07	9.91411E 07
9.90600E 07	5615.	140.0	3579.	-6.495	1.38800E 10	9.91428E 07	9.91428E 07
9.88252E 07	5609.	150.0	3516.	-6.124	1.48694E 10	9.91295E 07	9.91295E 07
9.85724E 07	5601.	160.0	3457.	-5.731	1.58564E 10	9.91026E 07	9.91026E 07
9.83085E 07	5594.	170.0	3402.	-5.311	1.68408E 10	9.90636E 07	9.90636E 07
9.80407E 07	5586.	180.0	3351.	-4.862	1.78226E 10	9.90142E 07	9.90142E 07

RDTR No. 157

MK 45-8		H50		WC	
CD	EMIN	TW	TC	HASL	0.
1.6500E .6	0.0200	22.50	3.14382		
OPT. ALT.	HT	0K			
3984.6	180.0				
AREA	RADIUS	TIME	HEIGHT	VELOCITY	AREA-TIME INTEGRAL
9.7275E 07	5565.	0.0	4762.	-10.522	0.0
9.78924E 07	5582.	10.0	4657.	-10.281	9.75841E 08
9.84104E 07	5597.	20.0	4556.	-10.030	1.95735E 09
9.88355E 07	5609.	30.0	4456.	-9.774	2.94358E 09
9.91724E 07	5619.	40.0	4360.	-9.514	3.93362E 09
9.94285E 07	5626.	50.0	4266.	-9.248	4.92662E 09
9.96058E 07	5631.	60.0	4174.	-8.976	5.92179E 09
9.97150E 07	5634.	70.0	4086.	-8.698	6.91839E 09
9.97564E 07	5635.	80.0	4000.	-8.413	7.91575E 09
9.97376E 07	5634.	90.0	3918.	-8.120	8.91322E 09
9.96664E 07	5632.	100.0	3838.	-7.818	9.61023E 09
9.95450E 07	5629.	110.0	3761.	-7.506	1.0903E 10
9.93850E 07	5625.	120.0	3688.	-7.182	1.1900E 10
9.91875E 07	5619.	130.0	3618.	-6.845	1.28938E 10
9.89580E 07	5612.	140.0	3551.	-6.492	1.38845E 10
9.87076E 07	5605.	150.0	3488.	-6.121	1.48728E 10
9.84397E 07	5598.	160.0	3429.	-5.728	1.58586E 10
9.81611E 07	5590.	170.0	3373.	-5.309	1.68416E 10
9.78831E 07	5582.	180.0	3322.	-4.860	1.78218E 10

MK 45-8

HSO

CD
1.6500E 06

EMIN
0.0200

OPT. ALT.
3984.6

BT
180.0

AREA	RADIUS	TIME	HEIGHT	VELOCITY	AREA-TIME INTEGRAL	AVERAGE AREA
9.69372E 07	5555.	0.0	4814.	-10.531	0.0	0.0
9.75979E 07	5574.	10.0	4709.	-10.289	9.72676E 08	9.72676E 07
9.81566E 07	5590.	20.0	4607.	-10.038	1.95145E 09	9.75724E 07
9.86226E 07	5603.	30.0	4508.	-9.782	2.93534E 09	9.78448E 07
9.90021E 07	5614.	40.0	4411.	-9.522	3.92347E 09	9.80867E 07
9.92969E 07	5622.	50.0	4317.	-9.256	4.91496E 09	9.82992E 07
9.95141E 07	5628.	60.0	4226.	-8.984	5.90902E 09	9.84836E 07
9.96596E 07	5632.	70.0	4137.	-8.705	6.90488E 09	9.86412E 07
9.97377E 07	5634.	80.0	4052.	-8.420	7.90186E 09	9.87733E 07
9.97568E 07	5635.	90.0	3969.	-8.127	8.89933E 09	9.88815E 07
9.97178E 07	5634.	100.0	3889.	-7.825	9.89671E 09	9.89671E 07
9.96319E 07	5632.	110.0	3812.	-7.512	1.08935E 10	9.90314E 07
9.95017E 07	5628.	120.0	3739.	-7.188	1.18891E 10	9.90760E 07
9.93351E 07	5623.	130.0	3669.	-6.851	1.28833E 10	9.91023E 07
9.91355E 07	5617.	140.0	3602.	-6.498	1.38757E 10	9.91118E 07
9.89140E 07	5611.	150.0	3539.	-6.126	1.48659E 10	9.91060E 07
9.86717E 07	5604.	160.0	3479.	-5.733	1.58538E 10	9.90864E 07
9.84180E 07	5597.	170.0	3424.	-5.313	1.68393E 10	9.90545E 07
9.81619E 07	5590.	180.0	3373.	-4.864	1.78222E 10	9.90120E 07

KUTR NO. 15/

RDTR No. 157

MK. 45-8		HSO		TW		WC	
CD	E ^{MIN}	BT	DK	HASL	Ü.	DK	17.50
1.6500E 06	0.0200	180.0	3.14382				
OPT. ALT.		BT					
3984.6							
AREA	RADIUS	TIME	HEIGHT	VELOCITY	AREA-TIME INTEGRAL	AREA	AVERAGE AREA
9.69763E 07	5556.	0.0	4808.	-10.530	0.0	0.0	0.0
9.76321E 07	5575.	10.0	4703.	-10.288	9.73042E 08	9.73042E 08	9.73042E 08
9.81887E 07	5591.	20.0	4601.	-10.037	1.95215E 09	9.76073E 07	9.76073E 07
9.86505E 07	5604.	30.0	4502.	-9.781	2.93634E 09	9.78780E 07	9.78780E 07
9.90231E 07	5614.	40.0	4405.	-9.521	3.92471E 09	9.81177E 07	9.81177E 07
9.93137E 07	5623.	50.0	4311.	-9.255	4.91639E 09	9.83278E 07	9.83278E 07
9.95268E 07	5629.	60.0	4220.	-8.983	5.91059E 09	9.85099E 07	9.85099E 07
9.96664E 07	5632.	70.0	4131.	-8.705	6.90656E 09	9.86651E 07	9.86651E 07
9.97425E 07	5635.	80.0	4046.	-8.419	7.90359E 09	9.87948E 07	9.87948E 07
9.97539E 07	5635.	90.0	3963.	-8.126	8.90106E 09	9.89006E 07	9.89006E 07
9.97136E 07	5634.	100.0	3883.	-7.824	9.89839E 09	9.89839E 07	9.89839E 07
9.96224E 07	5631.	110.0	3806.	-7.511	1.08951E 10	9.90461E 07	9.90461E 07
9.94889E 07	5627.	120.0	3733.	-7.187	1.18906E 10	9.90885E 07	9.90885E 07
9.93173E 07	5623.	130.0	3663.	-6.850	1.28847E 10	9.91127E 07	9.91127E 07
9.91169E 07	5617.	140.0	3596.	-6.497	1.38768E 10	9.91202E 07	9.91202E 07
9.88904E 07	5611.	150.0	3533.	-6.126	1.48669E 10	9.91124E 07	9.91124E 07
9.86456E 07	5604.	160.0	3473.	-5.733	1.58545E 10	9.90909E 07	9.90909E 07
9.83892E 07	5596.	170.0	3418.	-5.312	1.68397E 10	9.90571E 07	9.90571E 07
9.81308E 07	5589.	180.0	3367.	-4.863	1.78223E 10	9.90128E 07	9.90128E 07

RDTR No. 157

MK 45-8		HSO			
CD	EMIN	TW	WC		
1.650C ^E 76	0.0230	22.50	17.50		
OPT. ALT.	BT	OK	HASL		
3984.6	180.0	3.14382	0.		
AREA	RADIUS	TIME	HEIGHT	VELOCITY	AREA-TIME INTEGRAL
9.70590E 07	5558.	0.0	4796.	-10.528	0.0
9.77005E 07	5577.	10.0	4691.	-10.287	9.73798E 08
9.82477E 07	5592.	20.0	4589.	-10.035	9.76769E 07
9.86983E 07	5605.	30.0	4490.	-9.780	1.95254E 09
9.90649E 07	5615.	40.0	4394.	-9.519	2.93827E 09
9.93449E 07	5623.	50.0	4299.	-9.253	3.92708E 09
9.95501E 07	5629.	60.0	42C8.	-8.981	4.91913E 09
9.96818E 07	5633.	70.0	4119.	-8.703	5.91360E 09
9.97481E 07	5635.	80.0	4034.	-8.418	6.90976E 09
9.97521E 07	5635.	90.0	3951.	-8.125	7.90691E 09
9.97029E 07	5634.	100.0	3871.	-7.822	8.90441E 09
9.96051E 07	5631.	110.0	3795.	-7.510	9.90168E 09
9.94632E C7	5627.	120.0	3721.	-7.186	1.08982E 10
9.92856E 07	5622.	130.0	3651.	-6.849	1.18936E 10
9.90772E 07	5616.	140.0	3584.	-6.496	1.28873E 10
9.88453E 07	5609.	150.0	3521.	-6.125	1.38791E 10
9.85950E 07	5602.	160.0	3462.	-5.731	1.48687E 10
9.83316E 07	5595.	170.0	3406.	-5.311	1.58559E 10
9.80681E 07	5587.	180.0	3356.	-4.862	1.68406E 10
					1.78225E 10

RDTR No. 157

CD	EMIN	WC			
1.6500E 06	0.0200	22.50			
OPT. ALT.	BT	OK			
3984.6	180.0	3.14382			
MSO	TW	HASL			
	17.50	0.			
AREA	TIME	HEIGHT	VELOCITY	AREA-TIME INTEGRAL	AVERAGE AREA
9.70950E 07	5559.	0.0	4790.	-10.527	0.0
9.77370E 07	5578.	10.0	4685.	-10.286	9.74160E 08
9.82772E 07	5593.	20.0	4584.	-10.034	9.7715E 07
9.87234E 07	5606.	30.0	4484.	-9.779	9.79744E 07
9.90833E 07	5616.	40.0	4388.	-9.518	9.82067E 07
9.93618E 07	5624.	50.0	4294.	-9.252	9.84098E 07
9.95605E 07	5629.	60.0	4202.	-8.980	9.85850E 07
9.96863E 07	5633.	70.0	4114.	-8.702	9.87334E 07
9.97485E 07	5635.	80.0	4028.	-8.417	9.88563E 07
9.97491E 07	5635.	90.0	3945.	-8.124	9.89535E 07
9.96965E 07	5633.	100.0	3865.	-7.822	9.90322E 07
9.95955E 07	5630.	110.0	3789.	-7.509	9.90880E 07
88	5625.	120.0	3715.	-7.185	9.91242E 07
9.92697E 07	5621.	130.0	3645.	-6.848	9.91424E 07
9.90566E 07	5615.	140.0	3578.	-6.495	9.91438E 07
9.88195E 07	5608.	150.0	3515.	-6.124	9.91301E 07
9.85667E 07	5601.	160.0	3456.	-5.731	9.91027E 07
9.83028E 07	5594.	170.0	3401.	-5.311	9.90634E 07
9.80348E 07	5586.	180.0	3350.	-4.862	9.90137E 07

OPTIMUM IGNITION ALTITUDE = 4796. (WITHIN 6. FEET)

MK 45-8		VSF		TW		WC	
CD	EMIN	BT	DK	HASL	0.		
1.6500E 06	0.0200	22.50				17.50	
HC							
5635.1	180.0		3.14382				
AREA	RADIUS1	TIME	HEIGHT	VELOCITY	AREA-TIME INTEGRAL	AVERAGE ARE	
1.30062E 08	1552.	0.0	4796.	-10.528	0.0	0.0	
1.37437E 08	6619.	0.0	4691.	-10.287	1.33750E 09	1.33750E 08	
1.44172E 08	6767.	10.0	4589.	-10.035	2.74554E 09	1.37277E 08	
1.320.	6902.	20.0	4490.	-9.780	4.21817E 09	1.40606E 08	
1.50355E 08	1221.	30.0	4394.	-9.519	5.75022E 09	1.43756E 08	
1.56055E 08	1132.	40.0	4299.	-9.253	7.33712E 09	1.46742E 08	
1.61326E 08	1051.	50.0	4208.	-8.981	8.97480E 09	1.49580E 08	
1.66210E 08	977.	60.0					
1.70744E 08	910.	7428.	70.0	4119.	-8.703	1.06596E 10	1.52280E 08
1.74949E 08	849.	7511.	80.0	4034.	-8.418	1.23880E 10	1.54850E 08
1.78856E 08	793.	7587.	90.0	3951.	-8.125	1.41571E 10	1.57301E 08
1.82488E 08	742.	7658.	100.0	3871.	-7.822	1.59638E 10	1.59638E 08
1.85860E 08	696.	7723.	110.0	3795.	-7.510	1.78055E 10	1.61868E 08
1.88990E 08	654.	7784.	120.0	3721.	-7.186	1.96798E 10	1.63998E 08
1.91888E 08	615.	7840.	130.0	3651.	-6.849	2.15841E 10	1.66032E 08
1.94564E 08	580.	7891.	140.0	3584.	-6.496	2.35164E 10	1.67974E 08
1.97027E 08	549.	7938.	150.0	3521.	-6.125	2.54744E 10	1.69829E 08
1.99282E 08	520.	7981.	160.0	3462.	-5.731	2.74559E 10	1.71599E 08
2.01334E 08	494.	8021.	170.0	3406.	-5.311	2.94590E 10	1.73268E 08
2.03181E 08	472.	8056.	180.0		-4.862	3.14815E 10	1.74897E 08

RDTR No. 157

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Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified

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3. REPORT TITLE

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RDTR No. 157, 1 October 1969

5. AUTHOR(S) (First name, middle initial, last name)

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11. SUPPLEMENTARY NOTES

12. SPONSORING MILITARY ACTIVITY

13. ABSTRACT

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 This report presents a computer program written in Fortran IV for the IBM 360 that is a simulation of the illumination on the ground during the descent of an aircraft parachute flare from ignition to burn out. The effect of air density on the velocity is taken into account by a numerical technique. The illumination on horizontal and vertical surfaces on the ground are considered. For the surface of interest the area consisting of those points having at least a certain value of illumination is computed. The program searches for the ignition altitude for which this area is maximized over the burn time, finds the ignition altitude for which the flare burns out at a chosen altitude, or simulates the descent with ignition at a chosen altitude. Atmospheric transmission is not considered in this report.

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